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FAST NEUTRONS INCIDENT ON VANADIUM

by

Alan B. Smith, James F. Whalen, and Kenji Takeuchi

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Printed in the United States of America
Available from
Clearinghouse for Federal Scientific and Technical Information
National Bureau of Standards, U. S. Department of Commerce
Springfield, Virginia 22151
Price: Printed Copy \$3.00; Microfiche \$0.65

ARGONNE NATIONAL LABORATORY 9700 South Cass Avenue Argonne, Illinois 60439

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Reactor Physics Division

May 1969

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ABSTRACT

Total neutron cross sections and elastic and inelastic neutron scattering cross sections are experimentally studied. Total neutron cross sections are determined with good resolution (≥1 keV) from 0.1 to 1.45 MeV. Differential elastic and inelastic scattering angular distributions are measured at incident neutron energy intervals of ≈10 keV from 0.3 to 1.5 MeV with incident neutron resolutions of ~20 keV. The inelastic excitation of states at 330 ± 10 keV and 926 ± 10 keV is observed. The experimental results are interpreted in terms of the optical model and statistical concepts, inclusive of resonance width fluctuations and correlations. The observed intermediate structure is discussed in the context of strongly overlapping resonances and distributions in resonance widths and spacings and in terms of an intermediate optical model. Comparison is made with previously reported experimental values and with the pertinent contents of the evaluated data file, ENDF-B. Numerical tabulations of the experimental results are provided.

I. INTRODUCTION

The objective of this study was to improve the understanding of total neutron cross sections and of the elastic and inelastic scattering cross sections of vanadium at incident energies up to 1.5 MeV. Natural vanadium is monoisotopic, lies near the peak of the s-wave strength function, is magic in neutron number, and has relatively low-lying states, which are appreciably excited by inelastic neutron scattering processes. These collective properties are unusual, and many of them have been associated with the prevalence of intermediate structure in neutron processes. The relatively large inelastic excitations make possible the comparison of such intermediate structure between several reaction channels. The present work gave considerable attention to the experimental accuracies and energy resolutions in an effort to well define the energy-dependent structure.

In the discussion, Section II outlines the techniques used in the experimental portions of the study. The experimental results are presented in Section III and comparisons made with previously reported values. Section IV is devoted to the physical interpretation of the measured results. A broad energy average of the measured values is described in terms of a conventional optical potential² and statistical concepts³ inclusive of resonance width fluctuations. 4 The observed intermediate structure is discussed in the context of (a) strongly overlapping compound nucleus resonances,5 (b) fluctuations in widths and spacings of isolated or partially overlapping resonances, 6,7 and (c) an intermediate optical potential assuming reaction processes proceeding through "doorway" states. 8,9 Section V compares the results of the present study with the comparable physical quantities in the evaluated data file ENDF-B. 10 This comparison may prove of interest to the reactor physicist. Section VI consists of some brief summary remarks. The appendix presents experimental results in detailed tabular form.

II. EXPERIMENTAL METHOD

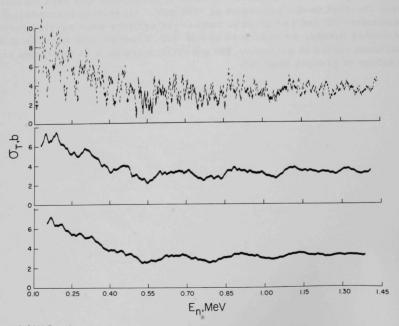
Fast-neutron time-of-flight techniques were used in all the scattering measurements and a portion of the total cross-section determinations. The experimental neutron-scattering apparatus, inclusive of a pulsed and bunched Van de Graaff accelerator, a multiangle detection system, on-line computer usage, and associated data-processing procedures, has been described in detail and will not be further defined here. 11,12 All measurements used the reaction $^7 \text{Li}(p,n)^7 \text{Be}$ as a neutron source, the intensity of which was monitored using "long counters" and proton-recoil scintillators. 13 The scattering samples were right cylinders (2.0 cm in diameter and 2.0 cm high) fabricated of natural vanadium metal. The chemical purity of the metal was $\approx 98\%$. Neutrons were incident upon the lateral surfaces of the scattering samples. All scattering measurements were made relative to the known differential elastic scattering cross sections of carbon and corrected for multiple scattering, incident-beam attenuation, and angular-resolution effects. 11,14

Total neutron cross sections were determined from neutron transmissions measured using a pseudowhite pulsed-source technique or the monoenergetic source method. ^{12,15} The latter method was used exclusively below incident neutron energies of ~500 keV. All neutron transmission measurements and reduction to total cross sections were carried out in an automated manner as described in Ref. 12. Transmission samples of natural vanadium varied in geometry, but generally were such as to provide transmissions of greater than 50%.

III. EXPERIMENTAL RESULTS

A. Total Neutron Cross Sections

The experimental total cross-section results in the measured interval 0.1-1.45 MeV are shown in the upper portion of Fig. 1. Numerical values are given in Table V (in the appendix). At incident neutron energies of <0.5 MeV, the experimental energy resolution was 1.5-2.5 keV. At higher energies, the velocity resolution was estimated to be $0.1\text{-}0.12\,\text{nsec/m}$, higher energies, the velocity resolution was estimated to the width of narfrom direct observation of the prompt gamma-ray burst and the width of narrow resonance peaks. The energy scale of the monoenergetic measurements was calibrated against the $^7\text{Li}(p,n)^7\text{Be}$ reaction threshold of $1.882\,\text{MeV}.^{16}$ Energy calibration errors in this method should have been less than 3 keV. The time-of-flight measurements were calibrated against the velocity of light and spot-checked using the above monoenergetic method. The error in the time-of-flight energy scale was judged appreciably less than 10 keV, with the larger uncertainties at the higher energies. The stated cross-section errors were derived from counting statistics. "In scattering" corrections were estimated, found small, and neglected.



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Fig. 1. Measured Total Neutron Cross Sections of Vanadium. Top, basic measured data; center, data averaged over a 50-keV interval; bottom, data averaged over a 100-keV interval.

Generally, the present results compared favorably with those obtained by other workers. ¹⁷ Values reported by Cabe $\underline{\text{et}}$ $\underline{\text{al}}$., in the interval 0.4-1.2 MeV follow the energy average of the present higher-resolution values. ¹⁸ The present work is consistent with the detailed results of Rohr and Friedland and of Firk $\underline{\text{et}}$ $\underline{\text{al}}$., reported for incident neutron energies of $\approx 200 \text{ keV}.^{19,20}$

B. Elastic Cross Sections

The differential elastic neutron-scattering cross sections were determined at incident neutron-energy intervals of ≈10 keV with an incident neutron-energy resolution of 20 ± 5 keV. The angular range of the measurements at each incident energy was from ~25 to ~155°, usually covered in eight angular intervals. Typical values of the laboratory scattering angles were 27, 38, 53, 69, 84, 114, 129, and 154°. The scattering angles were not always identical, but were carefully determined at each measurement. Angular resolutions varied, but were of the order of a few degrees. As indicated by the illustrative time spectra of Fig. 2, the scattered neutron velocity resolution of 1.5-2.0 nsec/m was sufficient to resolve the elastic scattered neutrons from inelastic scattered components.

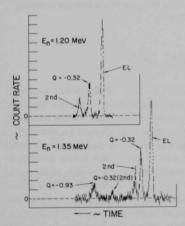


Fig. 2

Time-of-flight Spectra Obtained for Vanadium at a Laboratory Scattering Angle of 114° . Flight path was ~ 203 cm, and time per channel ~ 1.05 nsec. Elastic and inelastic scattered neutron groups are evident. Backgrounds have been subtracted, and vertical bars indicate standard deviation of respective points. No detector-sensitivity correction has been made. Reaction Q values associated with the various neutron groups are indicated in MeV.

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The experimental results were expressed in the following alternate forms:

$$\frac{d\sigma}{d\Omega} = \frac{\sigma}{4\pi} \left[1 + \sum_{i=1}^{4} \omega_{i} P_{i} \right],$$
and
$$\frac{d\sigma}{d\Omega} = \sum_{i=1}^{4} B_{i} P_{i},$$
(1)

where P_i are Legendre polynomials expressed in the laboratory system and σ , ω , and B are parameters derived by least-squares fitting Eq. 1 to experimentally measured differential distributions. The expansions of Eq. 1 were terminated at i=4, as the magnitudes of higher-order terms did not generally exceed their corresponding uncertainties. Expressed in either of the above forms, the results were descriptive of the measured data points (see Fig. 3), and parameter values obtained from measurements at slightly different incident energies or scattering angles were easily comparable. However, extrapolation of the results, expressed in the forms of Eq. 1, beyond the measured angular interval of ~25 to ~155°, is not necessarily valid.

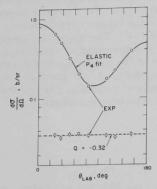


Fig. 3

Experimentally Observed Elastic and Inelastic Angular Distributions for Vanadium (data points). Solid curve is obtained from the least-squares fit of Eq. 1 to the experimental elastic scattering measurements. The dotted curve is an eye guide to the inelastic scattering angular distribution.

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As expected from the multiresonance nature of the total neutron cross section (see Fig. 1), the elastic scattering cross sections varied rapidly with incident energy. Small experimental variations in incident neutron energy and/or energy spread could, and did, result in quite different measured cross-section values. To provide consistent experimental results, the measured differential elastic cross sections were progressively averaged over a square energy increment with a width of several experimental resolutions. Figure 4 shows results obtained with a 50-keV averaging increment. Table VI (in the appendix) lists the numerical parameter values derived from the differential measurements. Assay of the experimental errors was complex and subjective. Generally, it was estimated that the elastic scattering cross sections were determined to an accuracy of ~8%, inclusive of uncertainties in the cross section of the carbon standard. The stated uncertainties in the angular-distribution coefficients represent standard deviations derived from the least-squares fitting procedures.

The elastic scattering results were generally consistent with the total cross section (see Section A above) as indicated in Fig. 5 and with the reported total scattering results of Ref. 14. The agreement between the present results and those obtained using a soft fission spectrum²¹ was less satisfactory.

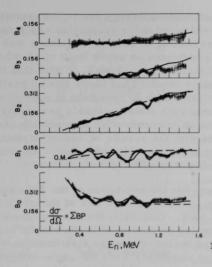


Fig. 4

Differential Elastic Scattering Cross Sections of Vanadium Given in the Format of Eq. 1. A 50-keV average of the measurements is indicated by the data points. The solid and dashed curves are the result of calculation (O.M.) as described in Section IV.A.

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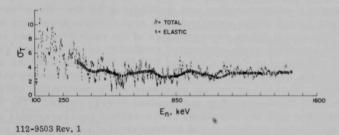


Fig. 5. Comparison of Experimental Total Neutron Cross Sections (vertical bars) and Total Elastic Scattering Cross Sections (boxes) of Vanadium

C. Inelastic Neutron Scattering

The inelastic excitation of states in vanadium at 330 ± 10 and 926 ± 10 keV was observed. The energy values were derived from the calibrated time scale of the velocity spectrometer and verified by observation of the excitation of the well-known 845-keV state in iron. These levels were attributed to reported states at 320 and 930 keV, respectively. The latter published values were accepted as the more accurate. Additional states in vanadium have been reported at 480, 645, and 1160 keV. Well in these experiments, any state at ~480 keV would have been partly obscured by the presence of elastically scattered neutrons from the second neutron group of the $^7\text{Li}(p,n)^7\text{Be}$ source reaction. However, it was felt that a cross section for the excitation of a 480-keV state of $\approx 10.0 \text{ mb/sr}$ would have resulted in an observable inelastically scattered neutron group. None was evident. Inelastic scattered neutrons (Q = -0.32 MeV) resulting from the second source group were clearly seen (see Fig. 2). A nearby neutron

group at a somewhat higher scattered neutron energy due to the excitation of a 645-keV state would have been observed if the respective cross section was $\gtrsim 2 \text{ mb/sr}$. No group corresponding to such a magnitude was observed. The experimental results indicated an upper limit of $\sim 4 \text{ mb/sr}$ for the excitation of any state in the vicinity of 1.16 MeV. Within this limitation, there was no evidence for such a level. Thus there was no positive evidence in the present experiments for states in vanadium at approximately 480, 645, and/or 1160 keV. If present, such states probably have spins and parities requiring $\ell \geq 2$ incident neutron momentum for appreciable excitation. This conclusion is consistent with the results of recent inelastic neutron-scattering measurements at higher incident energies and with the results of recent shell-model calculations.

The differential cross sections for the excitation of the 320- and 930-keV states were measured from several hundred keV of threshold to a maximum incident energy of 1.5 MeV. Generally the measurements were made at the same scattering angles as employed in the elastic scattering studies. Many of the measured inelastic angular distributions were essentially isotropic. (See Fig. 3, for example.) Thus the angle-integrated inelastic-excitation cross sections were reasonably obtained by averaging the differential measurements and multiplying by 4π . Even for the more anisotropic distributions observed, this approximate procedure was judged acceptable since it led to overestimates of the excitation cross sections by ≤5%. The resulting angle-integrated excitation cross sections are shown in Fig. 6 and listed in Tables VII and VIII (in the appendix). As was true for the elastic cross sections, the results varied with energy because of the partially resolved resonance structure and experimental uncertainties in the precise incident energy and incident-energy spread. The uncertainties associated with the individual cross-section measurements are complex composites of statistical and instrumental effects and were subjectively estimated. Those indicated in Fig. 6 and Tables VII and VIII are best estimates of the standard deviation inclusive of uncertainties in the reference standard cross section of carbon.

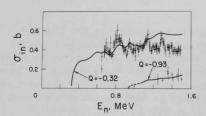


Fig. 6

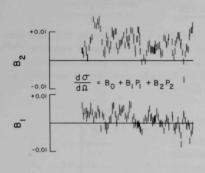
Measured Cross Sections for the Excitation of States in Vanadium at 0.32 and 0.93 MeV (crosses). The solid curve was obtained by calculation as described in Section IV.A. Estimated experimental uncertainties are indicated by vertical bars of the data crosses.

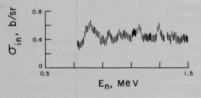
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The measured differential cross sections for the excitation of the 320-keV state were carefully assayed and the "better" angular distributions fitted, by the method of least squares, with the expression

$$\frac{d\sigma}{d\rho} = B_0 + B_1 P_1 + B_2 P_2. \tag{2}$$

The resulting B_i parameters were found to be very energy-dependent and were smoothed by averaging over a 20-keV incident energy increment.





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Fig. 7

Differential Cross Section for the Excitation of the 0.32-MeV State in Vanadium, Expressed in the Form of Eq. 2. Lowest plot: integrated cross section. Upper two plots: B1 and B2 coefficients of a Legendre expansion of the differential distributions. Data points (bars) do not indicate experimental uncertainties.

Figure 7 shows the resulting average energy dependence of these parameters. Though the parameters still vary appreciably, it is evident that (a) the cross section ($\sigma = 4\pi B_0$) has the same magnitude and energy dependence as that shown in Fig. 6, and (b) B1 tends to be less than B2, both on the average and in magnitude of the fluctuations. Further, there appears to be a qualitative correlation between fluctuations in B2 and B0. Instrumental effects may have contributed to the structure and anisotropy. Such perturbations were most likely at forward angles; thus most affect the B1 coefficient. Such a premise is not strongly supported by the results of Fig. 7. Coincidence may have led to measurements locally correlated with compound-nucleus resonance structure. resulting in systematic perturbation of measured magnitudes or angular distributions. The abundance of data and the random mode of its procurement over a several-year period made this hypothesis unlikely.

The present results can be compared with the few previously reported values. Towle reports cross sections for the excitation of the 320- and

930-keV states at incident energies of ~1.5 MeV similar to the results of the present work. ²⁵ Results of (n:n' γ) measurements by Mather et al., at 0.8, 1.0, and 1.5 MeV are consistent with the values obtained in the present work when cognizance is taken of the anisotropy of the emitted quanta and the effects of branching ratios. ²⁷ Barrows reports (n:n' γ) results at incident energies of 1.83 MeV and above. ²⁸ When extrapolated downward to the 1.5-MeV maximum energy of the present work, Barrows' results are slightly (~20%) higher than those reported here. This may in part be due to the use of the rapidly varying Fe(n; n' γ) (Q = -0.85 MeV) cross section as a reference standard in Barrows' work.

where

and

IV. PHYSICAL INTERPRETATIONS

A. Optical Model and Statistical Calculations

The optical model and statistical methods were used in the phenomenological interpretation and extrapolation of the experimental results.^{2,3,30,31} The potential employed was based upon the surface absorption model of Moldauer.³² The latter has been extended by Engelbrecht and Fiedeldey to an equivalent nonlocal potential of the form²⁹

$$\begin{split} V_{c}(\mathbf{r}) &= -(V + iU) \ f_{1}(\mathbf{r}) - if_{2}(\mathbf{r})W + V_{s0} \left(\frac{\hbar}{\mu_{\pi}c}\right)^{2} \underline{\sigma} \cdot \underline{\ell} \frac{1}{\mathbf{r}} \frac{\mathrm{d}f_{1}}{\mathrm{d}\mathbf{r}}, \\ f_{1}(\mathbf{r}) &= \left[1 + \exp\left(\frac{\mathbf{r} - R_{1}}{a_{1}}\right)\right]^{-1}, \\ f_{2}(\mathbf{r}) &= \exp\left[-\left(\frac{\mathbf{r} - R_{2}}{a_{2}}\right)^{2}\right], \\ R_{1} &= r_{1} + r_{0}A^{1/3}, \quad R_{2} = R_{1} + r_{2}, \\ r_{0} &= 1.16f, \quad r_{1} = 0.6f, \quad r_{2} = 0.5f, \\ a_{1} &= 0.62f, \quad a_{2} = 0.5f, \\ V^{*} &= V_{0} - 0.25E, \\ W^{*} &= W_{0} - 0.2E, \\ V_{s0}^{*} &= 7.0, \end{split}$$

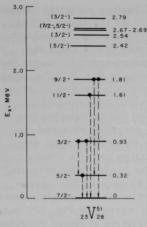
$$(3)$$

$$U^{*} &= 0.125E - 0.0004E^{2}. \end{split}$$

If we let E \rightarrow 0 and V \rightarrow 0 and set V_0 = 46 and W_0 = 14 MeV, Eq. 3 becomes the potential of Moldauer. This potential and the Hauser-Feshbach formalism give a good description of the low-energy observed elastic scattering (dashed curves of Fig. 4) and lead to calculated ℓ = 0 strength functions similar to those experimentally observed.

A detailed description of the observed structure in the elastic scattering was sought by varying V_0 and W_0 (U=0, and other parameters maintained constant) to obtain the best fit to the individual observed elastic scattering angular distributions.³³ The calculated results included compound

^{*}All energies in MeV.



112-9572

Fig. 8. Excited Structure of Vanadium 22

elastic scattering derived with the Hauser-Feshbach formula and the reported excited structure of vanadium²² (see Fig. 8). The angular distributions calculated using this fitting procedure were descriptive of measurement (Fig. 9) and followed the observed intermediate structure of the elastic scattering (see curves of Fig. 4). The Vo and Wo and associated transmission coefficients obtained from the fitting reflected the intermediate structure, fluctuating with energy as shown in Fig. 10.

The meaning of the above fluctuating parameters was not above question. However, above energies of about 1.1 MeV, Vo and Wo obtained from the fitting procedure approached asymptotic values of 43 and 8 MeV, respectively. Elastic scattering cross sections calculated from these "asymptotic parameters" were in reasonable agreement with experiment above ~0.8 MeV (see solid curves of Fig. 11), but the

agreement degenerated at lower energies, and the calculated $\ell = 0$ strength function was about half that reported from microscopic measurement.

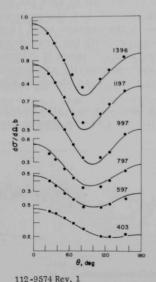
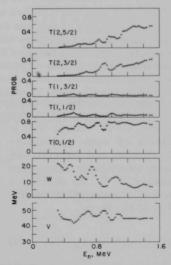
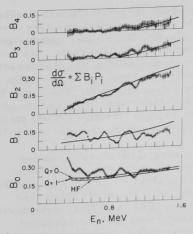


Fig. 9. Comparison of Measured (points) and Calculated (lines) Differential Elastic Distributions of Vanadium at Selected Incident Neutron Energies (keV)



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Fig. 10. Real (V) and Imaginary (W) Potential Values and Transmission Coefficients, T(l,j) Obtained by Fitting Eq. 3 to the Measured Elastic Scattering Cross Sections of Vanadium. See Section IV.A for discussion.



113-498

Fig. 11. Measured (crosses) and Calculated (curves) Elastic Distributions of Vanadium. The "asymptotic potential" form of Eq. 3 was used. The Hauser-Feshbach formalism was employed to estimate compound elastic contributions. Curves denoted as Q = 0 and Q = 1 were obtained by applying correction factors as described in Section IV.A. All calculated results lead to essentially identical B₁ → B₄ coefficients.

The fluctuating potential parameters obtained from the above fitting procedures and the Hauser-Feshbach formula were used to calculate the inelastic-excitation cross sections; the results are shown in Fig. 6. The calculated values qualitatively display structure similar to that experimentally observed, though the calculation was based upon the potential obtained entirely from the fit to the elastic data. Inelastic-excitation cross sections calculated from the "asymptotic potential" $(V_0 = 43, W_0 = 8)$ were in fair agreement with experiment at energies above ~1.0 MeV (solid curves of Fig. 12), but were less descriptive at lower energies. The low-energy discrepancies tended to be independent of potential and were evident in other reported calculations employing different potentials.25,68 Results of calculations made with changes of one unit of spin for both the 320- and the 930-keV states compared poorly with the experimental results. This, together with the previously reported evidence, 25 made it difficult to accept spin-and-parity assignments differing from those shown in Fig. 8.

Compound nucleus resonance widths fluctuate in a statistically describable manner, and transmission coefficients are no longer described

by $T=2\pi < \Gamma > D^{-1}$ where $T\to 1$. The effects of such resonance-width fluctuation and interference have been extensively discussed by Moldauer. ^{4,33,35} He derived a "corrected" transmission coefficient, θ_{α} , of the form

$$\theta_{\alpha} = 2Q_{\alpha}^{-1}[1 - (1 - Q_{\alpha}T_{\alpha})^{1/2}].$$
 (4)

For well-isolated resonances $\Gamma < <$ D, T is small and $\theta \rightarrow T$. Using the "asymptotic potential" and the correction factors of Eq. 4, we calculated both elastic and inelastic cross sections for the limiting

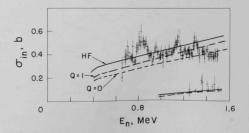
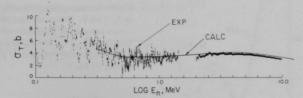


Fig. 12. Calculated (curves) and Measured (crosses) Cross Sections for the Excitation of the 0.32- and 0.93-MeV States in Vanadium. The interpretation of the calculated curves is discussed in Section IV.A.

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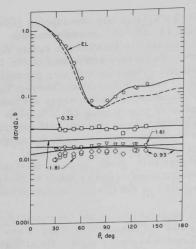
cases Q = 1 (isolated resonances) and Q = 0 (strongly overlapping resonances). The results are shown in Figs. 11 and 12. Results obtained with intermediate choices of the Q parameter lay between the limits set by the above extreme cases. The correction factors and choice of the Q parameter did not lead to calculated elastic scattering differing appreciably from that obtained with the Hauser-Feshbach formalism above. The effect of the correction factors on the calculated inelastic cross sections was appreciable (see Fig. 12), the corrected values lying 20-30% below the Hauser-Feshbach results and being in poorer agreement with experiment. These qualitative effects of the correction factors were not appreciably dependent upon the choice of the optical potential. Generally, comparison with present experiments gave little guidance as to desirability or magnitude of correction terms, though comparisons by other workers at higher energies indicated the desirability of the fluctuation correction. 25

It is interesting to examine the applicability of the "asymptotic potential" over a wide energy range, since the parameters of Eq. 3 are energy-dependent and the volume absorption becomes significant at higher energies. The calculated total neutron cross section compares well with experiment to 10.0 MeV (present work and Ref. 36), as illustrated in Fig. 13. The calculated elastic angular distributions are in agreement with experimental results reported at incident energies of 2.35, 3.0, and 7.05 MeV, as shown in Figs. 14, 15, and 16, respectively. 25,37,38 At 14.7 MeV. the agreement with experiment³⁹ is less satisfactory (see Fig. 17), although it is not clear whether the discrepancies are due to deficiencies in the calculation or experiment or both. Inelastic scattering calculated with the "asymptotic potential" and the Hauser-Feshbach formalism was in relatively good agreement with values measured²⁵ at 2.35 MeV (see Fig. 14). Generally, the form of Eq. 3 with the "asymptotic potential" parameters appears widely applicable to the calculation of total, elastic, and inelastic cross sections of vanadium at energies above about 0.8 MeV. The model is less successful at lower energies and certainly is not unique.



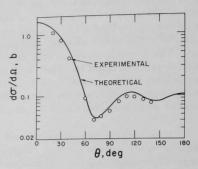
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Fig. 13. Measured and Calculated Total Cross Sections of Vanadium. Data for $E_{\rm n} \le 1.5$ MeV from present work, for $E_{\rm n} \ge 1.5$ MeV from the work of Galloway and Shrader. 36



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Fig. 14. Calculated Elastic and Inelastic Distributions of Vanadium and the Results Measured by Towle²⁵ at 2.35 MeV. Solid curves were obtained using the "asymptotic potential" form of Eq. 3. For comparison, dashed curves are those calculated in Ref. 40.



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Fig. 15. Elastic Angular Distribution of Vanadium Calculated Using the "Asymptotic Potential" Form of Eq. 3, Compared with the Measured Values of Becker at 3,0 MeV. 37

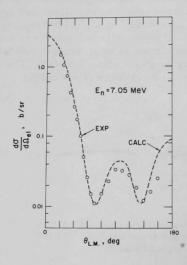


Fig. 16

Elastic Scattering from Vanadium at 7.05 MeV. Points are measured values reported by Holmqvist and Wiedling. ³⁸ The curve represents calculations using "asymptotic potential" of Eq. 3.

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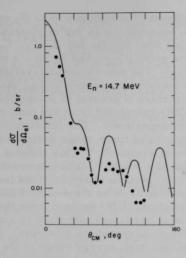


Fig. 17

Elastic Angular Distribution of Vanadium Measured at 14.7 MeV by Western et al., ³⁹ Compared with Results Calculated from Eq. 3.

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B. Correlations and Fluctuations

Correlations and fluctuations in the measured cross sections were examined with the intent of ascertaining the statistical properties of the observables and their physical significance. The interpretation took the forms of (a) a search for a quantitative measure of intermediate resonance structure, (b) an analysis based upon the premise of strongly overlapping resonances (Ericson fluctuations), 5,41,42 and (c) a derivation of average level density from fluctuations in widths and spacings of compound nucleus resonances. 6,7

1. Existence of Intermediate Resonance Structure

Intermediate structure can be attributed to measured cross sections by qualitative inspection. Such procedures can be deceptive. 43,44 A quantitative approach uses the function 7,44

$$C(R) = \frac{1}{N} \sum_{i=1}^{N} \left[\sigma(E_i) - \overline{\sigma(E_i)} \right]^2$$
 (5)

where

$$\overline{\sigma(E_i)} = \frac{1}{R} \int_{E_i-R/2}^{E_i+R/2} \sigma(E) dE.$$

C(R) increases with R, asymptotically approaching a constant value for R much larger than the average structure width of the fluctuating cross

section. In the presence of two very different fluctuation widths (Γ_1 and Γ_2 , where $\Gamma_1 << \Gamma_2$), C(R) increases with R, approaching an initial plateau value for $\Gamma_1 < R < \Gamma_2$ then rises to a second and final plateau for $R > \Gamma_2$. Γ_1 can be associated with the compound nucleus width $(\Gamma_{
m CN})$, and Γ_2 with a much larger intermediate resonance width ($\Gamma_{
m IS}$). The experimental resolution used in the present total cross-section measurements was $\lesssim \Gamma_{
m CN}$, sufficent to clearly indicate intermediate structure if present to an applicable extent. Figure 18 shows the function C(R) calculated from the total crosssection values determined in the present experiment. The function rises to a single oscillatory plateau characteristic of finite range deviations (FRD) inherent in the limited experimental sample. 45,46 This form of C(R) is consistent with a single average width of a few keV. The intermediate structure qualitatively apparent in the total neutron cross sections (see Fig. 1) must, if valid, be of such a magnitude as to be masked by FRD and statistical fluctuations in the C(R) distribution. C(R) derived from the measured elastic scattering cross sections oscillated with such an amplitude as to preclude any reasonable assay of intermediate structure. Such behavior was not unexpected, in view of the small energy range of the sample and the precision of the measurements. In the present experimental context, the use of the C(R) function for the assay of intermediate structure led to inconclusive results.

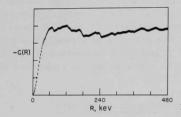


Fig. 18

Function C(R), Eq. 5, Evaluated from the Measured Total Neutron Cross Sections of Vanadium for 0 < R < 480 keV

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2. Limit of Strongly Overlapping Resonances, $\Gamma >> D$

Fluctuations have been observed in cross sections at energies at which the compound nucleus width is expected to greatly exceed the spacing $(\Gamma_{CN} >> D_{CN}).^{7,17,47-49}$ Ericson performed a theoretical study of these fluctuations and related observable quantities to average compound-nucleus properties. 5,41,42 As used here, his interpretation is based upon a number of assumptions, primary of which are: (a) The reactions are purely statistical, (b) $\Gamma >> D$, (c) $\Gamma^{J} \rightarrow \Gamma$ = a constant, (d) experimental resolutions $\langle \Gamma,$ and (e) no single- or several-particle resonance effects exist. Qualitatively, $\Gamma/D=n/2\pi$, where n is the number of effective exit channels. 50 In the present experiments, n was probably not $>>2\pi$; rather, $\ell=0$ strength functions 19 indicated that Γ/D was more nearly unity. $\Gamma^{J} \rightarrow \Gamma=$ constant implies a number of available exit channels and a large nuclear moment of inertia, not particularly characteristic of the present experiments. The effect of several particle resonances may be appreciable over much of the

measured energy interval (see Section IV.C below). Further, the experimental resolution used in the present total cross-section measurements was $\lesssim \Gamma$ only in limited and lower-energy regions. Thus an interpretation of the present work in the framework of Ericson fluctuations is open to considerable question. The approach is pursued here only in the spirit of a qualitative experimental assay.

Ericson derived the total cross-section correlation function⁵

$$\mathbf{F}(\epsilon) = \langle [\sigma(\mathbf{E} + \epsilon) - \langle \sigma(\mathbf{E}) \rangle] [\sigma(\mathbf{E}) - \langle \sigma(\mathbf{E}) \rangle] \rangle$$

$$\mathbf{F}(\epsilon) = \frac{\Gamma^2}{\epsilon^2 + \Gamma^2} \kappa \frac{D_0}{\pi \Gamma} \frac{(\pi \lambda^2)^2}{(2\mathbf{i} + 1)(2\mathbf{I} + 1)} \sum_{\ell} (2\ell + 1) \ \mathbf{T}_{\ell}^2,$$
(6)

where κ is a measure of the distribution of partial widths around the mean (~1.5 Porter-Thomas distribution⁵⁶), D^J = D₀/(2J+1), T_{ℓ} = optical model transmission coefficient, and i and I are the spins of the incident and target particles, respectively. In the ratio form,

$$C(\delta) = \frac{\langle \sigma(E + \delta) \cdot \sigma(E) \rangle}{\langle \sigma(E + \delta) \rangle \langle \sigma(E) \rangle} - 1 = \frac{1}{N} (1 - Y^2) \frac{\Gamma^2}{\delta^2 + \Gamma^2}, \tag{7}$$

where N = number of contributing independent channels and Y = the proportion of direct reactions. Equation 7 is independent of D_0 and κ .^{5,46} Further,

$$C(0) = \frac{1}{N} (1 - Y^{2}),$$
and
$$F(0) = \kappa \frac{D_{0}}{\pi \Gamma} \frac{(\pi \lambda^{2})^{2}}{(2i+1)(2i+1)} \sum_{\ell} (2\ell+1) T_{\ell}^{2}.$$
(8)

In the following, Eqs. 7 and 8 are used to obtain N and Γ from the measured cross sections and (with the T_{ℓ} values calculated using the "asymptotic potential" of Section IV.A) the value of D_0 . Corrections are made for the effect of the finite experimental resolution. 51,52 These corrections are not negligible, particularly at higher energies, where the assumptions of the theory become more applicable to the experiment.

The lower portion of Fig. 19 shows $C(\delta)$ calculated from the measured total cross sections. The function decreases rapidly from a maximum at δ = 0 to about half-magnitude, then slowly decreases in an oscillatory manner with increasing δ . The slow decrease at large δ is characteristic of a direct-reaction (DR) modulation, and the oscillations are attributed to the finite sample size. The DR modulation (shape scattering) could be removed from the measured data using results of a

suitable optical model calculation, but a model calculation of sufficient accuracy is difficult to achieve. As a phenomenological alternative, the DR component was determined by least-squares fitting the cubic

$$\delta_{\text{cal}} = a + bE + cE^2 + dE^3 \text{ (E in MeV)}$$
(9)

to the measured data. The order of the fit was such as to well describe the general energy dependence without unduly distorting the fluctuating structure. $\delta_{\mbox{\footnotesize{cal}}}$ was subtracted from the measured cross sections, and a positive constant added to ensure nonnegative values. The resulting "fluctuating cross section," shown in Fig. 20 together with the directly measured values, was used in subsequent correlation analysis.

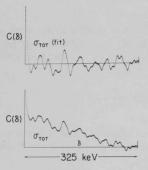
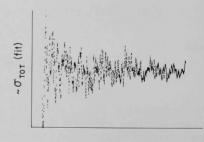
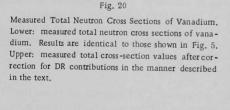


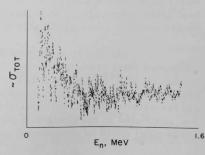
Fig. 19

 $C(\delta)$ Evaluated from Total Neutron Cross Sections of Vanadium. Lower: $C(\delta)$, Eq. 7, evaluated from the total neutron cross sections of vanadium. The effects of direct reactions and the finite sample range are evident. Upper: $C(\delta)$ evaluated from the total neutron corrected for direct reactions.

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 $F(\varepsilon)$ and $C(\delta)$ (from Eqs. 6 and 7) were evaluated from the fluctuating total cross section over the entire measured energy interval and a number of subintervals thereof. Typical of the results is $C(\delta)$ calculated for the entire interval shown in the upper portion of Fig. 19. FRD oscillations remain evident and are of an rms magnitude consistent with the estimates of Hall. 45,46 Neither in this example nor in any other $C(\delta)$ calculation was a significant deviation from a simple Lorentzian form noted as would be expected from appreciable intermediate resonance structure with a width $\Gamma_{IS} >> \Gamma_{CN}$. Table I summarizes C(0), F(0), Γ , and D_0 values, derived from the correlation analysis of the total cross sections, carried out over the entire measured interval and subintervals thereof using Eqs. 6-8. Uncertainties in the calculated C(0) and F(0) values are large; FRD alone led to standard deviations of 30% or more. The Γ values are remarkably consistent, and Do shows the expected energy dependence. However, D_0 tends to be an order of magnitude larger and Γ a factor of two to three larger than indicated by level density formulas, by results of detailed low-energy resonance studies, and by the analysis of average cross sections at low energies. 19,53,54 These discrepancies tend to compensate when the $\ell = 0$ strength function is estimated, resulting in a value about one-fifth of that reported from detailed resonance studies and about onethird to one-half of that obtained from average low-energy cross sections. In view of the inappropriateness of the theory in the present experimental context, the results are probably remarkable for their agreement with values obtained by other and more proper methods and tend to indicate that such analyses of total neutron cross sections are not sensitive to these theoretical concepts and underlying premises.

TABLE I. Results of Correlation Analysis of Measured Total Cross Sections

Energy Interval, MeV	0.1- 1.44	0.1- 0.42	0.21- 0.53	0.32- 0.64	0.43- 0.75	0.53- 0.86	0.64- 0.97	0.75- 1.07	0.85- 1.18	0.97- 1.29
C(0) C(0)	0.0378	0.101	0.0473	0.0353	0,0300	0.0234	0.0180	0.0152	0.0112	0.0081
F(0), b ²	1.103	3.03	1.384	0.957	0.848	0.647	0.546	0.439	0.346	0.235
Γ, keV	4.0	5.1	4.4	3.7	3.8	3.8	3.9	4.0	3.2	3.0
D ₀ , keV	410	540	304	223	225	189	171	162	115	83
$D = D_0/(2J + 1)^a$	49	65	36	26	27	23	20	19	13	10
$\Gamma/D _0 \times 10^{4a,b}$	0.96	1.5	2.0	2.0	1.8	2.0	2.2	2.2	2.4	2.8

^aAssuming 2J + 1 ≈ 8. bAll values corrected to 1 eV.

As is evident from Eq. 7, correlations are damped as the number of exit channels increases and thus should become more pronounced as the number of reaction channels is restricted. Therefore, to obtain more definitive results, $C(\delta)$ was evaluated for the $B\ell$ coefficients of the elastic channel and for the excitation cross section of the inelastic channel (Q = -0.32 MeV). Unfortunately, these correlation functions all showed strong FRD oscillations because of the limited extent of the available

sample. These oscillations and the experimental resolutions appreciably exceeding $\Gamma_{\rm CN}$ precluded any reasonable interpretation of the $C(\delta)$ derived from either the elastic or inelastic scattering measurements.

The cross correlation function

$$C_{ab} = \kappa G_{ab},$$
 where
$$G_{ab} = \frac{\langle \sigma_a \cdot \sigma_b \rangle}{\langle \sigma_a \rangle \cdot \langle \sigma_b \rangle} - 1$$
 and
$$\kappa = [C_a(0) \cdot C_b(0)]^{-1/2},$$

is of interest. 5,46 Cab was determined for the B\$\ell\$ coefficients of the elastic cross section, the elastic and total cross sections, and the elastic and inelastic (Q = -0.32 MeV) cross sections. The results are given in Table II. As expected, B0 (approximately elastic cross section) was strongly correlated with the total cross section (see Fig. 5). Between B\$\ell\$ values, only the B0 to B1 correlation appears significantly larger than FRD errors alone. This is in contrast to the concepts of Ericson, which indicate small correlations between even and odd B\$\ell\$ coefficients. There was no significant numerical correlation between elastic and inelastic cross sections, though experimental uncertainties and the limited range of the samples might have masked the small effect that seems qualitatively present from a visual inspection of the respective cross sections.

TABLE II. Cross-correlation Values

Processes	G _{ab} a,b	Cabb	
B_0 and σ_T	1.34×10^{-2} $\pm 0.36 \times 10^{-2}$	0.77	
B_0 and $\sigma_{\rm inel}$	0.18×10^{-2} $\pm 0.40 \times 10^{-2}$	0.088	
B_0 and B_1	1.4×10^{-2} $\pm 0.60 \times 10^{-2}$	-	
B_0 and B_2	-1.6×10^{-2} $\pm 1.2 \times 10^{-2}$	ilivana es	
B ₁ and B ₂	-1.5×10^{-2} $\pm 2.1 \times 10^{-2}$		

^aThe indicated uncertainties are lower limits, only pertaining to errors associated with the finite-energy range of the experimental samples.⁴⁶

bDefined by Eq. 10.

3. Cross-section Fluctuations and Distributions of Widths and $\overline{\text{Spacings}}$

In this section, structure in the measured total cross sections of vanadium is considered in the context of fluctuations in compound nucleus resonance spacings and widths after the manner of Carlson and Barschall⁷ and of Agodi and Pappalardo.⁶ It is assumed that the experimental resolution appreciably exceeds the average compound nucleus width, and experimental averages are constructed to ensure the validity of the premise. Within these averages, the interference between potential and compound scattering is neglected and the former's smooth energy dependence is removed by the cubic fitting procedure described by Eq. 9. It is further assumed that the partial widths are small compared to their spacings.

With the above premises, Carlson and Barschall derived the total cross section variance

$$S^{2} \; (\text{variance}) \; = \; (\pi \lambda^{2})^{2} \sum_{J\pi} \frac{g^{2}}{\langle N_{J\pi} \rangle} \Bigg[k_{W} \sum_{\ell s} \left(T_{\ell s}^{J} \right)^{2} \; + \; k_{n} \Bigg(\sum_{\ell s} \; T_{\ell s}^{J} \Bigg)^{2} \Bigg], \quad (11)$$

where g = (2J+1)/[2(2I+1)], $\langle N_{J\pi} \rangle$ is the average number of levels of a given $J\pi$ in the energy interval Δ , and $T_{\ell S}^J$ are transmission coefficients.³ The derivation makes use of the definitions

$$T_{\ell s}^{J} = 2\pi \langle \Gamma_{\ell s}^{J} \rangle / D_{J\pi}$$

$$k_{\rm W}$$
 = variance $\Gamma_{\ell s}^{\rm J}/\!\! \langle \Gamma_{\ell s}^{\rm J} \rangle$ = 2 for a Porter-Thomas distribution of widths,⁵⁶

and

$$k_n$$
 = variance $N_{J\pi}/\langle N_{J\pi} \rangle$ = 0.27 for a Wigner distribution of spacings.⁵⁷

Further, it is assumed that the distributions used in calculating the variances are independent of quantum number and that the widths associated with differing quantum numbers and spacings for the same quantum number are uncorrelated. Some of these assumptions are not without question. Fig. 8 If we separate the energy and spin dependence of the level density in the manner of Gilbert and Cameron, 54 < N $_{\rm J}\pi$ > / Δ = G(E) H(J π), Eq. 11 reduces to

$$S^{2}\Delta = (\pi\lambda^{2})^{2} \frac{1}{G(E)} \sum_{J\pi} \frac{g^{2}}{H(J\pi)} \left[k_{W} \sum_{\ell s} \left(T_{\ell s}^{J} \right)^{2} + k_{n} \left(\sum_{\ell s} T_{\ell s}^{J} \right)^{2} \right]. \quad (12)$$

Using $T_{\ell\,s}^{\,J}$ obtained from the "asymptotic potential" of Eq. 3, $H(J\pi)$ from Ref. 54, and S^2 determined from averages of measured values over the interval \triangle , we can obtain G(E). Table III gives the results for several energy intervals of the measured total cross sections and a number of averaging increments, Δ . In the table, the level density derived from the present experiments, ρ_{exp} = $G(E) \cdot H(J\pi)$, is compared with that given by the formula of Gilbert and Cameron (ρ_{theo}).⁵⁴ For averaging increments $\Delta >> \Gamma$ (i.e., $\Delta \stackrel{>}{\sim} 25 \; \mathrm{keV}$), the ρ_{exp} values obtained from the experiments are within a factor of two of those given by the density formula and are similar to values deduced from resonance studies at low energies. 19 The results were not particularly sensitive to the distributions of widths and spacings used in evaluating k_{W} and k_{n} . Assuming exponential distributions $(k_W = k_n = 1)$, or even neglecting width effects $(k_W = 0, k_n = 1)$, the results were similar to those obtained with Porter-Thomas and Wigner distributions. The $(k_w = 0, k_n = 1)$ assumption was that used by Agodi and Pappalardo. 6 Within the experimental uncertainties of 30-50%, the observed structure of the total cross section is consistent with the interpretation based upon recognized distributions of compound nucleus resonance widths and spacings. The distribution in spacings is a dominant factor, though the results are not sensitive to the detailed form of the distribution function.

TABLE III. Comparison of Experimentally and Theoretically Derived Level Densities

edes es el les es			Energy Interval, MeV	adverte de contra	
Averaging Increment		0.10-0.545 Av = 0.327	0.545-0.990 Av = 0.767	0.990-1.435 Av = 1.212	
	∫S²∆, b² MeV	7.49 x 10 ⁻³	1.8 x 10 ⁻³	0.56 x 10 ⁻³	
	ρ _{exp} , MeV ⁻¹	3.37×10^{3}	2.77×10^{3}	8.16×10^{3}	
$\Delta \cong 1-3 \text{ keV}^{a}$	ρ _{theo} , MeV ^{-1b}	1.27×10^{3}	1.73×10^{3}	2.34×10^{3}	
	$\rho_{\rm exp}/\rho_{\rm theo}$	2.6 (2.5, ^c 1.3 ^d)	1.59 (1.8, ^c 1.2 ^d)	3.47 (4.5, ^c 3.2 ^d)	
	$\int S^2 \triangle$, $b^2 \text{ MeV}$	1.65 x 10 ⁻²	0.38 x 10 ⁻²	0.13 x 10 ⁻²	
△ = 10 keV	ρ _{exp} , MeV ⁻¹	1.53×10^3	1.34×10^{3}	3.50×10^3	
	$\rho_{\rm exp}/\rho_{\rm theo}$	1.20 (1.1,° 0.6 ^d)	0.78 (0.9, 0.59 ^d)	0.78 (1.93,° 1.36d)	
	$\int S^2 \Delta$, $b^2 \text{ MeV}$	0.136 x 10 ⁻¹	0.477 x 10 ⁻²	0.216 x 10 ⁻²	
∆ = 25 keV	ρ _{exp} , MeV ⁻¹	1.85×10^{3}	1.09×10^{3}	2.14×10^{3}	
	$\rho_{\rm exp}/\rho_{\rm theo}$	1.46 (1.4,° 0.7 ^d)	0.63 (0.7,° 0.5d)	0.91 (1.2,° 0.8d)	
	∫S²∆, b² MeV	0.109 x 10 ⁻¹	0.495 x 10 ⁻²	0.265 x 10 ⁻²	
$\Delta = 50 \text{ keV}$	ρ _{exp} , MeV ⁻¹	2.37×10^{3}	1.05×10^3	1.76×10^3	
	$\rho_{\rm exp}/\rho_{\rm theo}$	1.82 (1.7, ^c 0.9 ^d)	0.61 (0.7, ^c 0.6 ^d)	0.74 (1.0,° 0.7 ^d)	
	S²∆, b² MeV	0.106 x 10 ⁻¹	0.546 x 10 ⁻²	0.234 x 10 ⁻²	
∆ = 75 keV	ρ _{exp} , MeV ⁻¹	2.30×10^{3}	0.95×10^{3}	1.97×10^{3}	
	Pexp/Ptheo	1.87 (1.7,° 0.9d)	0.549 (0.6,c 0.4d)	0.842 (1.1,° 0.8d)	

^aRaw experimental data, resolution as per Section III.A, ≳1 keV.

bCalculated from form of Gilbert and Cameron.54

^cRatio assuming exponential distribution of widths and spacings $(k_W=1, k_n=1)$. dRatio assuming only exponential spacing distribution $(k_W=0, k_n=1)$.

The expression $2\pi \langle \Gamma/D \rangle = T$ used in deriving Eq. 11 is known to be invalid when T approaches unity as it tends to in the present experiments. Considering resonance interference and \underline{S} matrix unitarity, Moldauer has derived the relation $2\pi \langle \Gamma/D \rangle = \ln \left[1/(1-T) \right]$, valid for large T.⁵⁹ The use of this relation increased the level densities derived from experiment (ρ_{exp} of Table III) by about a factor of three, to values appreciably larger than indicated by either level-density formulas or detailed resonance measurements. Such differences may, in part, be due to inappropriateness of Eq. 12 in the present experimental context. The equation is valid only for nonoverlapping resonances, and the Bethe randomness hypothesis^{6,55} is invoked to extend the validity to situations where partial widths alone are small compared to spacings. It is not clear that such an extrapolation is valid in the present experimental context.

C. The Intermediate Optical Model

The intermediate structure quantitatively evident in the energy-averaged total, elastic, and inelastic cross sections of vanadium can be characterized by a width, $\Gamma_{\rm IS}$, and a spacing, $D_{\rm IS}$, large compared to that of the compound nucleus and small relative to that of the single-particle or diffraction "giant resonances" (i.e., $\Gamma_{\rm CN} < \Gamma_{\rm IS} < \Gamma_{\rm SP}, D_{\rm CN} < D_{\rm IS} < D_{\rm SP}).$ The observed structure in elastic and inelastic scattering processes appeared correlated in scattering angle (see Figs. 7 and 21).

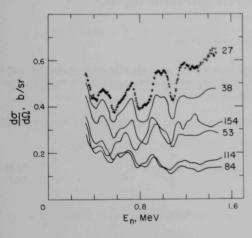


Fig. 21

Differential Elastic Neutron Scattering Cross Sections of Vanadium Observed at Laboratory Angles of 27-1549. The curves are derived from the measured values expressed in the form of Eq. 1. The results have been averaged over a 50-MeV energy interval to smooth local fluctuations. Actual measured values are indicated at 27°.

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Structure of the type observed here has been interpreted in terms of "doorway state" processess. 1,60,61 Many such interpretations tend to be qualitative comparisons with experiment. The "doorway state" has been quantitatively studied in the context of CN fine structure by Lejeune and Mahanx 69 and by Takeuchi and can be related to the properties of nuclear

structure in the manner of Lemmer and Shakin, for example. 10 Lipperheide, 9,64 Feshbach et al., 1 and Takeuchi have suggested an "intermediate optical model." The concept of an intermediate optical model has the advantages of simplicity of application and of avoiding excessive demands on experimental resolution. This concept is used in the present interpretation, the theoretical aspects of which follow Ref. 71.

Restricting the interpretation to the two open channels of s-wave elastic and inelastic scattering and assuming well-isolated doorway states and no direct reaction, the energy-averaged T-matrix for two open channels is 8,71

$$\left\langle T_{fi} \right\rangle = T_{fi}^{p} + 2\pi \sum_{s} S_{ff}^{p} \frac{\left\langle \chi_{f}^{(+)} PHd\Phi_{s} \right\rangle \left\langle \phi_{s} dHP\chi_{i}^{(+)} \right\rangle}{E - E_{s} - \Delta_{s} + \frac{i}{2} (\Gamma_{s}^{\downarrow} + \Gamma_{s}^{\uparrow})}, \tag{13}$$

where

 \textbf{T}^p and \textbf{S}^p are potential scattering T- and S-matrices,

 $\chi^{(+)}$ is the distorted wave satisfying outgoing-wave boundary conditions,

Es is the energy of the sth doorway state,

 Γ_s^{\downarrow} is the decay width of the sth doorway to the CN,

and

 Γ_s^{\uparrow} is the decay width to the continuum.

The width $\Gamma_{\mathbf{s}}^{\uparrow} = \Gamma_{\mathbf{s}1}^{\uparrow} + \Gamma_{\mathbf{s}2}^{\uparrow}$, where $\Gamma_{\mathbf{s}1}^{\uparrow}$ and $\Gamma_{\mathbf{s}2}^{\uparrow}$ are elastic and inelastic contributions, respectively, and P and d are projection operators to the open channel and the doorway, respectively.

The wave equation for complex potential interactions in the presence of doorways is $^{1,8,9,62-64}$

$$\left[PHP - \sum_{\mathbf{s}} f_{\mathbf{s}}(\mathbf{E}) \cdot PHd\phi_{\mathbf{s}} > \langle \phi_{\mathbf{s}} dHP - \mathbf{E} \right] \chi = 0, \tag{14}$$

where

$$f(E) = 1/(E - E_s + i \Gamma_s^{\uparrow}/2).$$

From this complex potential equation, a T-matrix, T^{cp}, can in principle be derived equivalent to the energy-averaged T-matrix of Eq. 13, and the total, absorption, elastic, and inelastic cross sections are obtained.⁷¹ The total cross section is proportional to the T-matrix and is given by^{8,9,64}

$$\langle \sigma_{\mathbf{c}}^{\mathrm{TOT}} \rangle = 2\pi \lambda_{\mathbf{c}}^{2} \left(-\mathrm{Im} T_{\mathbf{c}\mathbf{c}}^{\mathbf{c}\mathbf{p}}\right).$$
 (15)

The other cross sections follow from statistical considerations. The statistical properties of the T-matrix, $T=T^{DR}+T^{CN}$, have been extensively studied in the absence of a doorway. 4,66 In the presence of a doorway, the exact T-matrix can be written $T=T^{POT}+T^d+T^q.^1$ T^q has the same structure as T^{CN} , and T^d is assumed constant over an energy-averaging increment. Therefore $T^{POT}+T^d$ can be associated with T^{DR} , and T^q with T^{CN} . With these associations, the energy-averaged cross sections are given by 71

where

and

$$\langle \sigma_{cc'} \rangle = \sigma_{cc'}^{opt} + \sigma_{cc'}^{fl},$$

$$\sigma_{cc'}^{opt} = \pi \lambda_c^2 |T_{cc'}^{cp}|^2,$$

$$\sigma_{cc'}^{fl} = \pi \lambda_c^2 \frac{T_c^{CN} T_{c'}^{CN}}{\sum_{c''} T_{c''}^{CN}},$$

$$T_c^{CN} = 1 - \sum_{c''} |\delta_{c''} - i T_{cc''}^{cp}|^2.$$
(16)

In practice, the calculation of these quantities from the coupled complexpotential wave equation, Eq. 14, is difficult, and a simplified method is sought. For this purpose, the cross section is obtained from the following decoupled equations:

$$\left[P_1HP_1 - \sum_{\mathbf{S}} F_{\mathbf{S}1}(\mathbf{E})P_1Hd\phi_{\mathbf{S}} > \langle \phi_{\mathbf{S}}dHP_1 - \mathbf{E} \rangle \chi_1 = 0,$$
and
$$\left[P_2HP_2 - \sum_{\mathbf{S}} F_{\mathbf{S}2}(\mathbf{E})P_2Hd\phi_{\mathbf{S}} > \langle \phi_{\mathbf{S}}dHP_2 - \mathbf{E} \rangle \chi_2 = 0,$$

$$(17)$$

where P_1 and P_2 are projection operators for elastic and inelastic channels, respectively, and

$$\mathbf{F_{si}}(\mathbf{E}) = \frac{1}{\mathbf{E} - \mathbf{E_{s}} + \frac{\mathbf{i}}{2} (\Gamma_{s}^{\dagger} + \Gamma_{s}^{\dagger})_{j \neq i}}.$$
 (18)

and

The cross sections calculated from Eq. 17 can be compared with the energy-averaged cross sections of Eqs. 15 and 16.

The diagonal elements of the T-matrix derived from the decoupled Eqs. 17 are equivalent to those of T^{cp} obtained from the coupled Eq. 14, and the total cross section obtained from Eqs. 17 is equivalent to the energy-averaged total cross section. σ_{11}^{opt} of Eq. 16 is equal to that obtained from Eqs. 17, but the σ_{12}^{opt} of Eq. 17 is zero. Assuming Γ_{S1}^{\dagger} and Γ_{S2}^{\dagger} are equal, we can use transmission coefficients following from the decoupled equations to simply express elastic and inelastic cross sections in the following form: 71

$$\langle \sigma^{\text{el}} \rangle = \left\langle \sigma_{\text{OMHF}}^{\text{el}} \right\rangle - \frac{\Gamma_{\text{sl}}^{\dagger}}{\Gamma_{\text{sl}}} \sigma_{11}^{\text{HF}}$$

$$\langle \sigma^{\text{inel}} \rangle = \frac{\Gamma_{\text{s}}^{\dagger}}{\Gamma_{\text{s}}^{\dagger} + \Gamma_{\text{sl}}^{\dagger}} \frac{\Gamma_{\text{s}}^{\dagger} + \Gamma_{\text{s}}^{\dagger}}{\Gamma_{\text{s}}^{\dagger} + \Gamma_{\text{s}}^{\dagger}} \sigma_{\text{OMHF}}^{\text{inel}}.$$
(19)

Both of the above expressions are the familiar optical-model Hauser-Feshbach results modified by rather simple correction factors dependent on doorway-state widths.

Equations 17 have been interpreted as conventional optical-model equations, modified only by the presence of the energy-dependent factor $F_{si}(E)$. In the present analysis, an optical potential of the following form was chosen:

$$V^{\text{opt}} = -\overline{V} + i\overline{W} + \overline{V}_{S0} \underline{\ell} \cdot \underline{s} + F_1 + iF_2,$$
where
$$F_1 = \sum_{\mathbf{S}} S_{\mathbf{S}} \frac{E - E_{\mathbf{S}}}{(E - E_{\mathbf{S}})^2 + \left(\frac{\Gamma_{\mathbf{S}}^{\downarrow}}{2} + \frac{\Gamma_{\mathbf{S}}^{\uparrow}}{4}\right)^2}$$
and
$$F_2 = \sum_{\mathbf{S}} S_{\mathbf{S}} \frac{-\Gamma_{\mathbf{S}/2}^{\downarrow}}{(E - E_{\mathbf{S}})^2 + \left(\frac{\Gamma_{\mathbf{S}}^{\downarrow}}{2} + \frac{\Gamma_{\mathbf{S}}^{\uparrow}}{4}\right)^2},$$
(20)

 \mathbf{S}_s being the strength of interaction with the s doorway. The imaginary component, W, of Eq. 20 is due to reactions not proceeding through explicitly identified doorway states.

The potentials \overline{V} , \overline{W} , and V_{S0} were assumed to follow the spacial distributions of the phenomenological potential given in Eq. 3. The doorways are classified as the J^{π} each with associated strengths, resonant energies, Es, and widths, $\Gamma^{\dagger}_{J\pi}$. When averaged over energies large compared to those characteristic of the doorways, $F_1 \rightarrow 0$, $F_2 \rightarrow$ constant, and Eq. 20 reduces to the "conventional" optical potential. Other aspects of the intermediate potential, such as nonlocality and energy dependence, have been extensively discussed. 9,9

General application of Eq. 20 to the interpretation of experiment leads to the adjustment of a large number of parameters descriptive of each of a number of contributing doorway states. This would be true, for example, of charged-particle reactions at relatively high energies involving a number of angular momenta. The number of parameters is sharply reduced in the consideration of the present experiments at incident energies <1.0 MeV. $\ell=0$ processes are predominant with possible doorway configurations of and 4. Only the former can contribute to the inelastic channel (Q = -0.32 MeV, $\ell=0$). The present interpretation is further simplified by assuming that the reactions are spin-independent and that possible doorway states do not appreciably overlap. Both assumptions are qualitative approximations, but they do permit a simple interpretation of the measured results in terms of the above intermediate model.

The procedure followed was to select, by inspection, average \overline{V} and \overline{W} values and a limited number of doorways characterized by E_s , Γ_s^{\dagger} , and a strength, Ss, and calculate Vopt from Eq. 20 for comparison with the real and imaginary portions of the potential derived from a detailed fit to the measured elastic distributions (see Fig. 10). Commensurate with the assumption of isolated doorways and the known compound nucleus structure, the number of doorway states considered was restricted to \$5/MeV. Doorway parameters were suitably adjusted where indicated, and the above procedure was repeated until a reasonable agreement was achieved between Vopt and the experimentally derived potential. The "intermediate" potential was then used to calculate elastic and inelastic distributions for direct comparison with the measured values. Rather good results were obtained after three or four iterations. Typical are the comparisons of real and imaginary portions of Vopt and the experimentally derived potential shown in Fig. 22, and the elastic and inelastic results as measured and as calculated from Vopt shown in Fig. 23. The doorway parameters derived from these fitting procedures, assuming $\Gamma_{s1}^{\dagger} = \Gamma_{s2}^{\dagger} = \Gamma_{s}^{\dagger}/2$, are given in Table IV. To avoid an upper-energy "end effect," three additional doorways were postulated and distributed uniformly between 1.1 and 1.6 MeV. Their effect on the calculated results below ~0.8 MeV was small. No additional doorway states were assumed below the minimum experimental observed energy of ~0.3 MeV.

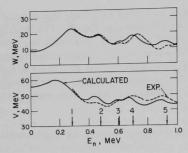


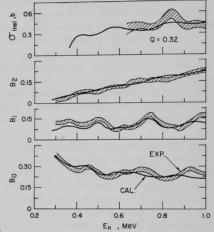
Fig. 22

Real (V) and Imaginary (W) Portions of the Intermediate Optical Potential (Eq. 20), Calculated, Compared with the Phenomenological Optical Potential Derived from a Fit to the Measured Elastic Scattering Distributions, EXP. Positions of doorway states are indicated by arrows referring to Table IV values.

113-1872



Comparison of Experimental Elastic Scattering Angular Distributions and Inelastic Cross Sections, EXP., of Vanadium with Those Calculated from the Intermediate Optical Potential and Statistical Theory, CAL.



113-1871

TABLE IV. Doorway Potential Parameters Used with Eq. 20a

No. of State	E _s , MeV	$\Gamma_{\rm s}^{\uparrow}/\Gamma_{\rm s}^{\downarrow}$	Γ _s (tot), MeV	T ₀ Peak	Strength, MeV ²
1	0.28	0.3	0.31	0.74	1.80
2	0.48	2.02	0.135	0.88	0.70
3	0.60	3.52	0.11	0.54	0.22
4	0.70	1.99	0.17	0.89	0.99
5	0.93	2.33	0.27	0.78	0.97

^aCalculations used \overline{V} = 48.0 MeV and \overline{W} = 6.5 MeV.

Vopt qualitatively describes the features of the experimentally derived potential (see Fig. 22) with the more serious differences at the higher incident energies, where $\ell \neq 0$ contributions are of increasing importance. Vopt also provides a similar qualitative description of the measured elastic angular distributions (see Fig. 23). The structure of the B, coefficient is particularly well portraved by calculations based upon Vopt. The correlation between measured and calculated inelastic scattering is less satisfactory. but the former did not appreciably extend over much of the appropriate energy range of Vopt. From the doorway parameters (listed in Table IV) and T_0 calculated at the peaks of the respective states, the ratios $\Gamma^{\uparrow}/\Gamma^{\downarrow}$ and the total doorway width $\Gamma = \Gamma^{\uparrow} + \Gamma^{\downarrow}$ can be evaluated, 1,8,71 with the results given in Table IV. Though speculative, the quantities are of magnitudes commensurate with the estimates of theory. 1,8 Averaging F1 and F2 of Eq. 20 over energy intervals much greater than \(\Gamma_{IS}\) or Dis leads to a Vopt that reasonably describes the measured results averaged over a 200-keV energy interval. However, the s-wave strength function calculated from Vopt for E - 0 is approximately a factor of seven smaller than indicated by direct observation or systematics. This may reflect the presence of doorways near zero or negative energy not identified by the present experiments.

The above interpretation is consistent with the presently observed structure in the total and elastic scattering cross sections of vanadium. This interpretation is reasonably free of gross assumptions or the use of an unduly large number of parameters. It is a logical development of the general optical potential. The interpretation provides qualitative knowledge of the properties of doorway resonances without detailed understanding of CN resonance structure. Indeed, the method precludes a direct correlation between explicit CN and doorway resonance parameters, in the manner of Monahan and Elwyn. ⁶⁷

V. COMPARISON WITH ENDF-B

Since a motivation of the present work was the provision of fast-neutron data for reactor design, it is instructive to compare the present results with the pertinent contents of the Evaluated Nuclear Data File-B (ENDF-B). 10,68

As indicated in Fig. 24, the total cross sections determined in the present work compare reasonably well with the ENDF-B values. The ENDF-B evaluation was finished before the completion of the present work and therefore does not show the recently measured detailed resonance behavior. At higher energies, the ENDF-B values are in good agreement with the work of Galloway and Shrader36 and extrapolate well during the uncertain interval from 1.5 to 2.0 MeV. Throughout the range 0.3-10.0 MeV, the ENDF-B values are closely followed by the total cross section calculated using the potential of Section IV.A, as shown in Fig. 25. Elastic scattering cross sections contained within the ENDF-B file are in a somewhat different format from that used in Section III.B. However, when transformed to the present base (format of Eq. 1), they are remarkably descriptive of the experimental values, as indicated in Fig. 26. Such differences as do exist are largely in regions of strong fluctuations. Figure 27 compares experimental and ENDF-B inelastic scattering values. The evaluation relied to an appreciable extent upon optical-model and statistical calculations, and these show the same tendency toward low cross sections for the excitation of the 320-keV state, particularly near threshold, noted in Section IV.A. At higher energies, ENDF-B and experimental values reported by Towle are in good agreement.25

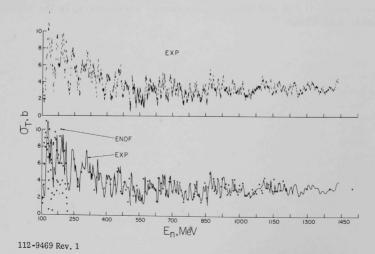


Fig. 24. Total Cross Sections of Vanadium Derived from Present Work (top) and ENDF-B Data¹⁰ (lower)

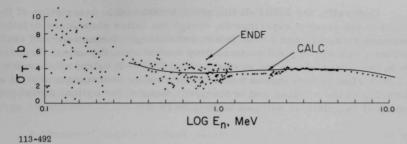


Fig. 25. Total Cross Sections, Calculated as Described in Section IV.A,

Compared with ENDF-B Values

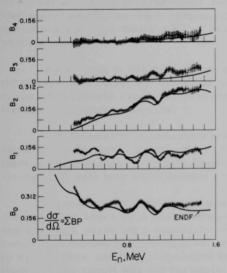


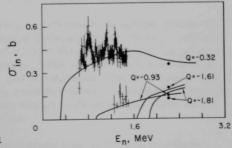
Fig. 26

Elastic Scattering Cross Sections of Vanadium Determined in the Present Work (data points) and the Values Given by ENDF-B (solid curves)

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Fig. 27

Measured and ENDF-B Inelastic Excitation Cross Sections of Vanadium. Data below 1.5 MeV (crosses) are from present work, Solid data circles are values reported by Towle. 25 Solid curves are ENDF-B values. Reaction Q values are indicated.



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Generally, the ENDF-B file gives a reasonable description of the results of the present experiments, though the latter show more detailed resonance structure and result in somewhat larger inelastic cross sections. Whether these are critical matters may depend upon the use of the information in the design of reactor systems. The ENDF-B values at energies >1.5 MeV closely correspond to other reported measurements of total and scattering cross sections and to the predictions of the optical model and statistical calculations outlined in Section IV.A.

VI. CONCLUDING REMARKS

The observed total, elastic and inelastic scattering cross sections were characterized by both a fine and intermediate energy-dependent structure. Though of good resolution, the results did not provide a definition commensurate with compound-nucleus resonance analysis, and the interpretation was confined to the intermediate structure and the average energy dependence of the observed quantities.

A phenomenological optical-potential was shown descriptive of total and elastic scattering cross sections of vanadium over a wide energy range. Results of calculations based upon this potential and statistical theory were qualitatively descriptive of the observed inelastic scattering, but quantitatively deviated from measurement, particularly near the reaction thresholds. Consideration of alternative spin-parity assignments and/or the effects of resonance width fluctuations failed to enhance the agreement with the present experiments.

An attempt to use correlation analysis in a quantitative assay of the observed intermediate structure was inconclusive because of the effects of the finite sample range, the presence of direct reactions, and the uncertainties of the measurements.

The suitability of Ericson's concepts in the context of the present experiments is highly questionable. However, an interpretation based upon them led to reasonable strength functions, though the derived Γ and D were inconsistent with both experimental evidence and the basic premise ($\Gamma \gg D$).

An experimental interpretation of the observed structure in the total cross section based upon known compound-nucleus distributions in widths and spacings, assuming a nonoverlapping of partial resonance widths, resulted in compound-nucleus-level densities similar to those predicted by systematics and by extrapolation from detailed low-energy resonance studies. The result was not particularly sensitive to the form of the distributions of either Γ or D, or even to the omission of the former.

The results of calculation using an intermediate optical potential, based upon the premise of a few isolated doorway states, were in qualitative agreement with the experimental elastic distributions and the phenomenological potential derived therefrom. This intermediate model used relatively few doorway parameters, and comparison with experiment led to parameter values of the magnitude expected from theoretical estimates. A wider application of the method may assist in determining some of the statistical properties of doorway states.

The latter two of the above interpretations of the intermediate structure appear physically applicable and result in qualitative agreement

with experiment. The approaches are not unique, and other interpretations have led to similar qualitative successes.^{59,67} The various interpretations are not necessarily mutually exclusive and may each appreciably contribute to the physical reality.

The present work indicates that the evaluated vanadium data (ENDF-B) often used in reactor calculations is reasonably representative of microscopic measurement and should be suitable for many applied studies. As increasingly fine energy groups are used in macroscopic calculation, it may become desirable to refine the evaluated data to take more cognizance of the observed fine-resonance structure. Further, it may be desirable to revise the evaluated file to bring it into better agreement with the results of the present and other recent studies of the inelastic neutron-scattering cross sections of vanadium. Such revisions will be appreciable near the first inelastic threshold (Q = -0.32 MeV).

APPENDIX

Tabulations of Measured Cross Sections

Tables V-VIII are provided for the use of those individuals interested in numerical values of the experimental quantities, either for pure or applied reasons.

TABLE V. Observed Total Neutron Cross Sections of Vanadium

E _n , keV	σ _T , b	dσ _T , b	E _n , keV	σ _T , b	$d\sigma_T$, b
100.79	4.58	.09	101.89	3,51	.09
102.89	2.82	.09	103.89	3.15	.09
104.89	2.39	.09	105.89	1./8	.09
106.89	1.99	.09	107.99	2.55	.09
108.99	1.65	. 09	109.99	1,91	.09
110.99	1.97	. 09	111.99	2,38	.09
112.99	3.54	.09	113.99	3.07	.09
114.99	4.36	.09	110.99	5.46	.09
116.99	5.61	.09	11/.99	6.18	.09
118.99	6.99	.09	120.09	1.19	.09
121.09	8.61	. 09	122.09	9.05	.09
123.09	9.64	. 09	124.09	10.20	.09
125.09	10.32	. 49	120.09	10.90	.09
127.09	10.18	.09	128,10	10.69	.09
129.10	12.19	. 09	130.10	9.12	.09
131.09	8.46	. 49	132.09	/.51	.09
133.09	8.04	. 09	134.09	5.54	.09
135.09	6.02	.09	130.09	6,96	.09
137.09	7.13	. 09	138.09	1.10	.09
139.19	8.17	. 09	140.19	8.70	.09
141.19	8.93	.09	142.19	8.57	.09
143.20	7.70	.09	144.19	5.49	.09
145.19	5.07	. 09	140.19	5.87	.09
147.19	5.40	. 09	145.19	4.99	.09
149.19	3.61	. 49	150.19	3,52	.09
151.19	2.94	. 09	152,19	3,63	.09
153.19	5.13	. 09	154.19	5.58	.09
155.19	5.67	.09	156.19	5.46	.09
157.19	4.74	.09	150.19	4.47	.09
159.19	5.28	.09	160.19	4.94	.09
161.19	6.65	. 49	162.19	/.88	.09
163.19	8.43	. 49	164.19	9.24	.09
165.19	9.39	.09	160.19	9.24	.09
167.19	9.49	. 49	108.19	9.17	.09
169.29	8.17	. 09	170.29	6.63	.09
172.29	0.01	.09	173.29	6.13	.09
174.29	5.99	. 49	175.29	5./4	.09
176.29	6.04	.09	17/.49	5.86	• 09
178.49	5.89	.09	179.49	6.06	.09
180.49	5.96	. 49	181.49	6.28	.09

E _n , keV	σ _T , b	dσ _T , b	E _n , keV	σ_{T} , b	dσ _T , b
		. 09	183.49	6.53	.09
182.49	6.57	.09	185.49	1.31	.09
184.49	7.50	. 09	18/.59	8.49	.09
186.49	7.93		189.59	9.29	.09
188.59	9.49	.09	191.29	8.65	, 09
190.59	8.19	. 09	193.59	7.36	.09
192.59	7.17	.09	195.59	9.61	.09
194.59	9.47	.09	197.59	8.39	.09
196.59	8.95	.09	199.59	7.65	.09
198.59	6.81	.09	201.59	5.38	.09
200.59	6.38	.09	203.59	4.52	.09
202.59	5.11	.09		6.48	.09
204.59	5.41	.09	205.09	8.73	.09
206.59	7.64	.09	20/.59	7,55	.09
208.59	8.69	.09	209.59	6.21	.09
210.59	7.04	.09	211.59	6.04	.09
212.59	6.39	.09	213.59		
214.59	6.57	.09	215.59	6.42	.09
216.59	6.53	.09	217.59	3,83	.09
218.59	4.02	.09	219.59	3.54	• 0 9
220.59	3,93	.09	221.59	3.15	.09
222.59	3,05	. 09	223.59	2.99	.09
224.59	2.53	.09	225.59	2.65	.09
226.59	3.08	.09	227.59	3.29	.09
228.59	3.70	.09	229.59	3.14	.09
230.59	4.79	. 09	231.59	5.62	• 0 9
232.59	7.01	. 09	233.59	6.57	.09
234.59	6.70	.09	235.09	1.55	.09
236.59	7.28	.09	231.59	7,61	.09
238.59	7.94	.09	239.59	7.10	.09
240.59	7.89	.09	241.59	7,38	.09
242.59	7.08	. 49	243.59	7,26	.09
244.59	7.07	.09	245.59	7.02	.09
246.59	6.97	.09	247.59	5,60	.09
248.59	5.65	.09	249.59	5./4	.09
250.59	5.54	. 49	251.69	5,18	.09
252.69	5.21	. 09	253.69	5./3	.09
254.69	5.33	. 09	255.69	5.61	.09
256.69	5.88	. 19	257.69	5.05	.09
258.69	5.16	.09	259.69	4.72	.09
260.69	3.92	.09	261.69	3.57	.09
262.69	3.06	.09	263.70	3.67	.09
264.69	4.31	. 09	265.70	4.42	.09
266.69	4.18	. 49	261.69	4,43	.09

E _n , keV	σ _T , b	$d\sigma_T$, b	E _n , keV	σ _T , b	dσ _T , b
268.69	4.30	. 49	269.69	3.69	.09
270.69	2.90	. 49	271.09	2.48	.09
272.70	2.54	. 49	273.69	2,19	.09
274.69	2.58	. 09	275.69	4.50	.09
276.69	5.13	. 49	277.69	5.15	.09
278.69	5.45	. 09	279.69	5,02	.09
280.69	5.88	.09	281.69	5.99	.09
282.69	6.30	.09	285,69	6.49	.09
284.69	6.11	.09	285./0	5,83	.09
287.69	5.35	. 19	288.69	5.40	.09
289.69	5.85	. 09	290.69	5,68	.09
291.69	5.69	.09	292.69	5.65	.09
293.69	5.71	.09	294.69	5,93	.09
295.69	5.26	.09	296.69	5,44	.09
297.69	5.40	.09	290,69	5.46	.09
299.69	5.97	.09	300.09	5.80	.09
301.69	6.12	. 49	302.69	6.04	.09
303.89	7.60	. 09	304.09	6.48	.09
305.89	7.01	.09	306.89	1.56	.09
307.89	7.36	. 49	508.89	1.55	.09
309.89	6.62	. 09	510.69	5.46	.09
311.89	4.58	.09	512.89	4,60	.09
313.89	5.19	.09	314.89	4.99	.09
315.89	4.98	.09	510.69	4,63	.09
317.89	5.59	.09	518.89	6,40	.09
319.89	6.47	.09	320.99	6.01	.09
321.99	5.94	.09	322.99	5.03	.09
323.99	4.45	.09	324.99	4.11	.09
325.99	3.49	. 49	526.99	4.79	.09
327.99	5.08	. 09	328.99	5.01	.09
329.99	4.51	. 09	330.99	3,97	.09
331.49	5.22	. 49	332.49	5.94	.09
333.49	6.44	.09	334.49	5.87	.09
335.49	5.71	.09	330.49	5.21	.09
337.49	5.63	.09	338.49	4.95	.09
339.49	5.39	. 09	340.49	5.03	.09
341.49	4.65	.09	342.49	4.66	.09
343.49	4.69	. 09	344.49	4.47	.09
345.49	4.16	.09	346.49	3.75	.09
347.49	3.33	.09	348.49	3.29	. 09
349.49	2.74	. 49	350.49	2.26	.09
351.49	3.87	. 09	352.49	4.54	.09
353.49	4.70	.09	354.49	5,31	.09

					1 1
E _n , keV	σ _T , b	$d\sigma_{\mathrm{T}}$, b	E _n , keV	σ _T , b	dσ _T , b
		"10	356.49	6,42	.09
355.49	5,67	.09	358.49	5.93	.09
357.49	6.58	.09	360.49	4./0	.09
359.49	5.24	.09	362,59	4.50	.09
361.59	4.42	.09	364.59	5.93	.09
363.59	4.21	. 49		4.11	.09
365.59	4.29	. 49	366.60	4.96	.09
367.59	4.76	.09	368.59	5.39	.09
369.59	4.99	.09	370.59	4.74	.09
371.59	5.00	. 49	372.59	4.47	.09
373.59	4.90	. 49	374.59	4.53	.09
375.60	4.42	. 49	376.59	3.11	.09
377.59	3.68	.09	578.59	2.99	.09
379.59	3.06	.09	380.59	3.13	.09
381.60	3.05	.09	382.59	3.13	.09
383.59	2.88	.09	384.59	3.04	
385.59	3.10	.09	386.59	2.45	• 09
387.59	2.09	.09	388.59	2.08	.09
387.89	1.96	. 09	388.89	2.44	.09
389.89	2.56	. 49	390.89	3,33	.09
392.89	2.53	. 09	393.89	2.99	.09
394.89	3.76	.09	395.89	4.49	.09
396.89	4.71	. 09	391.89	4.81	.09
398.89	4.16	.09	399.89	4.83	.09
400.89	4.07	. 09	401.89	4.52	.09
402.89	4.01	.09	403.90	4.58	.09
404.89	4.13	.09	405.89	4.60	.09
406.89	4.70	.09	407.89	4.24	.09
408.89	4.44	.09	409.90	4.47	.09
410.89	4.22	.09	412.09	4,38	.09
413.09	4.23	.09	414.10	2.86	.09
415.09	2.56	.09	416.09	2.01	.09
417.09	2.41	.09	418.09	2.27	.09
419.09	2.09	. 09	420.09	1.87	.09
421.09	2.27	.09	422.09	2,13	.09
423.09	2.20	.09	424.09	2.12	.09
425.09	2.23	. 09	426.09	2,97	.09
427.09	2.84	.09	428.09	3,03	.09
429.09	3.43	.09	430.09	3,24	.09
431.09	3.33	.09	432.09	3,53	.09
431.09	3.79	.09	434.09	4.20	.09
435.09	4.58	.09	436.09	4.65	.09
437.09	5.09	. 49	438.09	4,57	.09
			440.09		
439.09	4.59	.09	770.09	3,28	.09

E _n , keV	σ _T , b	dσ _T , b	E _n , keV	σ_{T} , b	do _T , b
441.09	2.36	. 49	442.09	2.27	.09
443.09	2.71	.09	444.09	5.57	.09
445.10	3.43	. 09	446.09	5.07	.09
447.09	3.57	.09	448.09	3.52	.09
449.09	4.27	.09	450.09	5,12	.09
451.09	5.36	.09	452.09	5.44	.09
453.09	5.38	.09	454.09	5.11	.09
455.09	5.30	.09	456.09	5.18	.09
457.09	4.82	. 09	458.09	4.52	.09
459.09	5.00	.09	400.09	5.03	.09
461.09	5.38	.09	462.09	5.92	.09
463.09	5.19	.09	464.09	4.06	.09
465.09	4.01	.09	466.09	4.08	.09
467.09	3.47	. 09	468.09	3.16	.09
469.09	3.19	.09	470.09	2.33	.09
471.09	2.53	. 49	472.09	2.47	.09
473.09	2.25	. 09	474.09	2.33	.09
475.19	2.37	. 49	470.19	2.99	.09
477.19	3.49	.09	478,19	3.02	.09
479.19	3.18	. 09	480.19	3.36	.09
481.19	3.73	.09	482.19	4.09	.09
483.19	3.95	.09	484.19	3.66	.09
485.19	3.89	. 09	480.19	3.67	.09
487.19	3.80	. 09	488.19	3.48	. 09
489.19	3.57	.09	490.19	3,23	.09
491.19	3,66	.09	492.19	3.52	.09
493.19	3.47	.09	494.19	3.40	.09
495.19	3.13	.09	496.19	3.10	.09
497.19	3.17	.09	498,19	3,12	.09
499.19	3.35	.09	500.19	2.56	.09
501.19	2.60	.09	502.19 504.19	1./0	.09
503.19	2.04	.09	500.19	1.65	.09
505.19	1.36	.09	506.08	.67	.15
505.58	1.41	.14	20/.08	.67	.15
506.58	1.35	.14	200.09	1.20	.14
507.59	.72		204.10	1.06	.14
508.60	1.38	.14	214./5	4.46	.10
514.21	4.66	.10	212./6	4.35	.10
515.24	4.12	.11	210./9	4.11	.10
516.28	3.73	.11	51/.03	3.07	.11
517.31		.11	210,08	5.44	.10
518.35	3.29	.12	219.92	3.36	.10
519.40	2.66				

					1 h
E _n , keV	σ _T , b	dσ _T , b	E _n , keV	$\sigma_{\mathbf{T}}$, b	dσ _T , b
			520.97	2.17	.11
520.44	2.75	.11	522.02	3.30	,10
521.49	3.16	.10	523.08	3.65	.10
522.55	3.25	.11	524.13	3.25	.10
523.60	3.65	.10		3.24	.10
524.66	3.61	.10	525.20	2.99	.11
525.73	3.28	.10	526.26	2.65	.11
526.79	3.14	.10	52/.33	2.59	.11
527.86	3.18	.10	528.40	2.29	.11
528.94	2.10	.12	529.47	1.75	.12
530.01	2.03	.11	530.55	1,63	.12
531.09	1.62	.12	531.63		.14
533.26	1.08	.14	533.81	1.15	.13
534.35	1.44	.13	534.90	1.70	,13
535.44	1.83	.13	555,49	1.89	
536.54	2.14	.12	531.09	2,36	•12
537.64	2,58	.12	530.19	2.61	•12
538.74	2.91	.11	534.30	2.91	•11
539.85	2.94	.12	240.41	3,20	.11
540.96	3.05	.11	541.52	2,86	.11
542.08	2.72	.11	542.05	2.45	.12
543.19	2.18	.12	545.15	1,97	.12
544.31	2.29	.12	544.87	2.32	.12
545.44	2.50	.11	546,00	2.35	.11
546.57	1.73	.12	54/.13	1.65	.12
547.70	1.75	.12	548.26	1.67	.12
548.83	1.68	.12	549.40	2.62	.11
549.97	2.79	.11	550.04	3,11	.10
551.11	3.14	.10	551.69	3.18	.10
552.26	2.69	.11	552.83	2.96	.10
553.41	2.36	.11	253.98	2.26	.11
554.56	2.20	.11	252,14	1.79	.12
555.72	1.47	.12	550.50	1,58	.12
556.88	1.53	.12	221.46	1.56	.12
558.04	1.43	.12	250.03	1.64	.12
559.21	1.74	.12	259.80	1,50	.11
560.38	1.50	.12	260.97	1,99	.11
561.56	1.91	.11	262.15	2.28	.11
562.74	2.54	.10	263,33	2.26	.11
563.92	1.82	.11	264.21	2.11	
565.11	1.72	.11	262./0	1,54	•11
566.30	1.35	.12	266.89		•11
567.49	1.11	.12		1.51	.12
568.69	1.43	.12	568.09	1.25	•12
,,,,,	1.40	• 1 4	264.29	1.56	.12

TABLE V (Contd.)

E _n , keV	σ _T , b	$d\sigma_T$, b	E _n , keV	σ _T , b	dσ _T , b
569.89	1.11	.12	570.50	1.31	.12
571.10	1.64	.11	571./0	1,68	.11
572.31	2.08	.11	572.92	1.67	.11
573.52	2.45	.10	574.13	2.90	.10
574.74	3,23	. 49	575.35	4.07	,09
575.96	4.40	. U8	576.57	4.40	.09
577.19	4.50	. U8	571.00	4.47	.08
578.42	4.23	. 49	579.03	4./1	.08
579.65	4.35	.08	580.27	4,29	.08
580.89	3.78	. 09	581.51	3.57	.09
582.13	2.94	.10	582.15	2.53	.10
583.38	1.96	.11	584.00	2,27	.15
584.63	2.42	.10	282.25	2.24	.10
585.88	2.15	.11	586.51	2.40	.10
587.14	2.62	.10	587.17	2.59	.10
588.40	3.02	.10	589.03	3.07	.10
589.67	3.69	.09	590,30	5.62	.09
590.94	3.29	. 09	591.57	3.53	. 09
592.21	3.10	.10	592.85	3,05	.09
593.49	2.03	.10	594.13	3.05	.09
594.77	3.31	.09	595.42	3,63	.09
596.06	4.18	.08	596.70	4.16	.09
597.35	4.18	.09	598.00	4.56	.08
598.65	4.12	.09	599,30	4.00	.09
599.95	3.98	. 09	600.60	3.49	.09
601.25	3.25	.09	601.90	3.48	.09
602.56	3.39	. 09	603.21	3.23	.09
603.87	3.20	.09	604.53	2.95	.09
605.19	3.18	. 09	605.85	3.35	.09
606.51	2.98	.09	607.17	3.06	.09
607.84	2.92	.09	000.50	2.97	.09
609.17	3.33	. 09	609.83	3.17	.09
610.50	3.69	.09	611.17	3.83	.09
611.84	3.59	.09	612.51	3.63	.09
613.19	3.51	.09	613.86	3.10	.09
614.53	2.88	.09	612.21	3.17	.09
615.89	2.98	.09	616.57	3.15	.09
617.24	3.43	.09	617,92	3.34	.09
618.61	3.34	.09	619.29	3,30	.09
619.97	3.49	.09	520.66	3,29	.09
621.34	2.81	.09	022.03	2.63	.09
622.72	2.76	.09	623.41	3.06	.09
624.10	2.73	. 09	624.79	3.00	,

E _n , keV	σ _T , b	dσ _T , b	E _n , keV	σ _T , b	$d\sigma_{\mathbf{T}}$, b
11.			626.18	3.16	.09
625.49	3.27	.09	62/.57	2.10	.10
626.88	2.48	.10		2.10	.10
628.27	2.12	.10	628.97	1.97	.10
629.67	1.81	.10	630.37	1,32	.11
631.07	1.46	.15	631./8	1,97	.10
632.48	1.59	.10	633.19	3.05	.09
633.89	2.57	. 09	634.60	5,49	.09
635.31	3.63	.08	636.02	4.07	.08
636.74	3.77	. 09	637.45	4,51	.08
638.16	4.15	.08	638.88		.08
639.60	4.49	.08	640.32	4.16	.08
641.04	3.98	.08	641.76	3.90	
642.48	3.96	.08	643.20	3.40	.09
643.93	3.00	. 09	644.65	2.81	.09
645.38	2.42	.10	646.11	2.13	,10
646.84	2.34	.15	647.57	2.29	.15
648.30	2.35	.11	649.03	2,29	•11
649.77	2,76	.11	650.00	3,43	.10
651.24	3.55	.10	651.98	3./0	.10
652.72	3.83	.10	655,46	4.10	.09
654.20	4.15	. 09	654.94	4.50	.09
	4.97	.09	650.43	4.59	.09
655.69	3.66	.1ù	651.95	3.16	.10
657.18	3.20	.10	659.43	3.40	.10
658.68	3.77	.10	660.94	3.92	.09
660.18	4.31	.19	662.45	4.62	.09
661.69	4.63	. 19	663,96	4.54	.09
663.21	4.49	.09	005,49	4.16	.09
664.72	4.01	.09	66/. 11	5.48	.10
666.25	2.77	.10	668,55	2.44	.11
667.78	2.42	.11	670.08	2.04	,11
669.31	2.12	.11	671.63	2.37	.11
670.86		.11	673.18	2.66	.11
672.40	2.29	.10	674.73	3.00	.10
673.95	3.10		676.29	2,27	.11
675.51	3.03	.10	677.86	2.00	,11
677.07	2.69	.10			.11
678.64	2.15	.11	679.43	2.01	.12
680.21	1.74	.12	681.00	1,86	.10
681.79	2.41	.11	682.58	2.65	
683.38	3.15	.10	686,56	4.18	.09
687.36	4.17	.09	686.16	4.28	.09
688.97	4.57	.08	689,17	4.50	.09
690.58	4.80	.08	691.38	4.47	.09

6					da h
E _n , keV	σ _T , b	$d\sigma_{T}$, b	E _n , keV	σ _T , b	do _T , b
692.19	4.41	.09	693,00	4.00	.09
693.81	3.93	.09	694.63	3.37	.10
695.44	3.25	.10	696.26	2.81	.10
697.07	2.93	.10	697.89	2.60	.10
698.71	2.53	.10	699.54	2.37	.11
700.36	2.83	.10	701.18	2,94	.10
702.01	3.24	. 09	/02.84	3,37	.09
703.67	3.35	.09	704.50	4,23	.09
705.33	3.68	.09	706.16	3,61	.09
707.00	3.91	.09	707.83	3.90	.09
708.67	4.21	.08	709.01	4.33	.08
710.35	4.01	.09	/11.19	3,52	.09
712.04	2.97	.10	/12.88	3,11	.10
713.73	2.70	.10	/14.58	2.55	.10
715.43	2.54	.10	716.28	3.07	.09
717.13	3.04	.10	/1/.99	3,06	,10
718.85	3.08	.10	719.70	3,51	.09
720.56	3.14	.09	721.42	3,77	.09
722.29	3,51	.09	/23,15	3./4	.09
724.02	3.21	.09	724.88	2,58	.10
725.75	2.40	.10	126.62	2.84	.10
727.50	3.02	.10	/28.37	3.38	.09
729.24	3.77	.09	730.12	3.79	.09
731.00	3.65	.09	/31.08	3,82	.09
732.76	3.74	.09	/33.64	3,25	.09
734.53	3.13	.09	132.42	3.37	.09
736.30	3,13	. 09	/37.19	3,42	.09
738.09	3.52	.09	738.98	3.22	.09
739.87	2.96	.09	740.77	3.01	.09
741.67	2.64	.10	142.57	2.56	.10
743.47	2.87	.09	744.37	2.38	
745.28	2.19	.10	/46.18	2.02	.10
747.09	1.60	.11	/48.00	1,47	.15
748.91	1.71	.11	/49.82	1,46	.15
750.74	1.62	.15	/51.65	2,27	.09
752.57	1.74	.09	155.34	2.58	.09
754.41	2.33	.09	/57.19	2.76	.08
756.26	3.02	.08	/59.05	2.85	.08
758.12	2.82	. U 8	760.91	2.93	.08
759.98	2.61	.08	762.78	2,63	.08
761.85	2.69	.08	164.66	1,56	.09
763.72	2,20	.09	/60.25	1./8	.09
765.61	1.70	.09	700175	-11.0	

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						dor, b
767, 50 767, 50 767, 50 769, 39 769, 39 769, 39 771, 30 2, 35 1, 94 772, 25 2, 57 773, 21 2, 72 1, 08 1, 74, 17 2, 47 1, 09 773, 21 2, 76 1, 08 1, 78, 09 1, 77 1, 05 3, 46 1, 08 1, 78, 02 3, 18 1, 08 775, 13 2, 76 1, 08 1, 78, 02 3, 79 1, 07 1, 05 3, 46 1, 08 1, 78, 02 3, 79 1, 07 1, 05 3, 46 1, 08 1, 09			1- h	F., keV	o _T , b	do.T.
767.50	En, keV	$\sigma_{\mathbf{T}}$, b	doT, b	-11'		0.0
767.50 769.39 1.94 771.30 2.35 0.99 772.25 2.57 0.88 775.13 2.76 0.88 0.76.09 3.18 0.87 775.13 2.76 0.88 0.76.09 3.18 0.87 775.13 2.76 0.88 0.76.09 3.18 0.87 0.77 0.95 3.46 0.88 0.78.02 3.79 0.77 0.78.99 3.70 0.77 0.79.96 3.79 0.87 0.88 0.81.90 0.88 0.88 0.89 0.88 0.88 0.89 0.88 0.89 0.88 0.89 0.88 0.89 0.89	**			768.44	1.92	
769,39	767.50	1.68			2.25	
771.30		1.94		770.25		
773.21						.09
775.13		2.72			3.18	.08
777.05		2.76	.08		3.70	.07
778.99			.08		3.79	. 07
780.93			.07			
782.87			.08			
784.83						
786.79 786.79 786.79 786.79 1.86 1.86 1.4 789.75 1.86 1.4 789.75 1.86 1.4 791.73 790.74 1.91 792.72 2.57 0.9 794.72 2.63 0.9 797.72 2.52 0.9 796.72 2.43 0.9 797.72 2.52 0.9 798.72 2.44 0.9 799.73 2.85 0.9 798.72 2.44 0.8 801.75 3.83 0.8 802.76 3.72 0.8 803.78 804.79 2.86 0.9 804.79 2.86 0.9 807.85 0.08 807.85 0.08 807.85 0.08 807.85 0.08 807.85 0.08 809.90 3.68 0.08 810.93 3.19 0.08 811.96 2.93 0.9 813.00 2.51 0.9 814.03 2.43 0.9 815.07 2.28 0.9 815.07 2.28 0.9 815.07 2.28 0.9 816.10 2.41 0.9 817.14 2.72 0.9 818.19 2.89 0.9 819.23 2.56 0.9 821.32 2.43 0.9 822.38 2.48 0.9 823.43 2.42 0.9 823.43 2.42 0.9 824.48 0.9 825.54 1.84 0.9 827.66 1.77 0.0 828.79 1.98 1.5 834.06 2.30 0.11 835.14 2.44 0.11 836.22 2.77 0.11 837.30 3.11 0.844.91 3.12 0.10 849.31 3.54 0.9 851.52 0.9 851.52 0.9 851.41 0.9 851.52			.08			
788.76 788.76 1.86 1.4 791.73 2.04 1.91 790.74 1.91 792.72 2.57 794.72 2.63 0.9 795.72 2.22 794.72 2.63 0.9 797.72 2.52 0.9 798.72 2.44 0.9 799.73 2.85 0.9 798.72 2.44 0.9 800.74 3.46 0.8 801.75 3.83 0.8 802.76 3.72 0.8 804.79 2.86 0.9 807.85 3.10 0.8 806.83 3.37 0.8 806.83 4.00 0.8 807.85 3.10 0.8 806.83 4.00 0.8 807.85 3.10 0.8 809.90 3.68 0.8 801.96 809.90 3.68 0.8 801.96 809.90 3.68 0.8 801.96 809.90 3.68 0.8 801.96 809.90 3.68 0.8 801.96 801.96 801.96 801.96 801.96 802.76 3.72 0.8 802.76 3.72 0.8 803.88 0.9 803.88 0.9 803.88 0.9 804.03 809.90 8			. 09	787.78		
790.74				189.15		
792.72		1 01		791.73		
794.72 2.63 .09 795.72 2.32 .09 796.72 2.43 .09 797.72 2.32 .09 798.72 2.44 .09 799.73 2.85 .09 800.74 3.46 .08 801.75 3.83 .08 802.76 3.72 .08 803.78 3.10 .08 804.79 2.86 .09 802.81 3.07 .08 806.83 3.37 .08 807.85 3.24 .08 808.88 4.00 .08 809.90 3.68 .08 810.93 3.19 .08 811.96 2.93 .09 815.07 2.28 .09 814.03 2.43 .09 815.07 2.28 .09 816.10 2.41 .09 817.14 2.72 .09 818.19 2.89 .09 821.32 2.56 .09 820.28 2.54 .09 823.43 2.44				795.72		
796.72 2.43 .09 797.72 2.85 .09 798.72 2.44 .09 799.73 2.85 .09 800.74 3.46 .08 801.75 3.83 .08 802.76 3.72 .08 803.78 3.10 .08 804.79 2.86 .09 805.81 3.07 .08 806.83 3.37 .08 807.85 3.04 .08 808.88 4.00 .08 817.96 2.93 .09 810.93 3.19 .08 817.96 2.93 .09 813.00 2.51 .09 814.03 2.43 .09 815.07 2.28 .09 816.10 2.41 .09 817.14 2.72 .09 818.19 2.59 .09 819.23 2.56 .09 820.28 2.54 .09 821.32 2.43 .09 824.48 2.16 .09 823.43 2.94				795.72		
798.72 2.44 .09 799.73 2.59 108 800.74 3.46 .08 801.75 3.83 .08 802.76 3.72 .08 803.78 3.10 .08 804.79 2.86 .09 805.81 3.07 .08 806.83 3.37 .08 807.85 3.54 .08 608.88 4.00 .08 809.90 3.68 .08 810.93 3.19 .08 811.96 2.93 .09 813.00 2.51 .09 814.03 2.43 .09 815.07 2.28 .09 816.10 2.41 .09 817.14 2.72 .09 818.19 2.59 .09 817.23 2.56 .09 820.28 2.54 .09 821.32 2.43 .09 822.38 2.48 .09 823.43 2.42 .09 824.48 2.16 .09 825.54 1.84				797.72	2,32	
798.72 2.44 .08 801.75 3.83 .08 800.74 3.46 .08 803.78 3.10 .08 802.76 3.72 .08 805.81 3.07 .08 804.79 2.86 .09 807.85 3.54 .08 806.83 3.37 .08 807.85 3.54 .08 608.88 4.00 .08 809.90 3.68 .08 608.88 4.00 .08 809.90 3.68 .08 608.88 4.00 .08 809.90 3.68 .08 810.93 3.19 .08 811.96 2.93 .09 810.93 3.19 .08 811.96 2.93 .09 813.00 2.51 .09 814.03 2.43 .09 815.07 2.28 .09 818.19 2.89 .09 817.14 2.72 .09 820.28 2.54 .09 821.32 2.43				199.73	2,85	
800.74 3.40 .08 803.78 3.10 .08 802.76 3.72 .08 805.81 3.07 .08 804.79 2.86 .09 805.85 3.54 .08 806.83 3.37 .08 807.85 3.54 .08 608.88 4.00 .08 809.90 3.68 .08 810.93 3.19 .08 811.96 2.93 .09 813.00 2.51 .09 814.03 2.43 .09 815.07 2.28 .09 816.10 2.41 .09 815.07 2.28 .09 818.19 2.89 .09 817.14 2.72 .09 818.19 2.89 .09 817.14 2.72 .09 820.28 2.54 .09 821.32 2.43 .09 822.38 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 823.43 2.42 .09 824.48 2.16 .09 825.54 1.84 <td< td=""><td></td><td></td><td></td><td></td><td>3,83</td><td>,08</td></td<>					3,83	,08
802.76 3.72 .09 805.81 3.07 .08 804.79 2.86 .09 807.85 3.54 .08 806.83 3.37 .08 807.85 3.54 .08 608.88 4.00 .08 807.85 3.54 .08 810.93 3.19 .08 811.96 2.93 .09 813.00 2.51 .09 814.03 2.43 .09 815.07 2.28 .09 816.10 2.41 .09 815.07 2.28 .09 818.19 2.89 .09 817.14 2.72 .09 818.19 2.89 .09 817.14 2.72 .09 820.28 2.54 .09 821.32 2.43 .09 822.38 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 823.43 2.42 .09 824.48 2.16 .09 825.54 1.84 .10 826.72 1.75 .10 827.66 1.77 <td< td=""><td></td><td></td><td></td><td></td><td>3,10</td><td>.08</td></td<>					3,10	.08
804.79 2.88 806.83 3.37 .08 807.85 3.54 .08 608.88 4.00 .08 809.90 3.68 .08 810.93 3.19 .08 811.96 2.93 .09 813.00 2.51 .09 814.03 2.43 .09 815.07 2.28 .09 816.10 2.41 .09 817.14 2.72 .09 818.19 2.89 .09 817.23 2.56 .09 820.28 2.54 .09 821.32 2.43 .09 822.38 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 822.54 .09 820.28 2.54 .09 827.66 1.77 .10 824.72 1.75 .10					3.07	.08
806.83 3.37 .08 809.90 3.68 .08 810.93 3.19 .08 811.96 2.93 .09 813.00 2.51 .09 814.03 2.43 .09 815.07 2.28 .09 816.10 2.41 .09 817.14 2.72 .09 818.19 2.89 .09 819.23 2.56 .09 820.28 2.54 .09 821.32 2.43 .09 822.38 2.48 .09 823.43 2.42 .09 824.48 2.16 .09 825.54 1.84 .10 826.60 2.11 .09 827.66 1.77 .10 826.60 2.11 .09 827.81 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 837.30 3.11 .10 836.22 2.77 .11 837.30 3.11 .10 842.72 3.19 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>.08</td></td<>						.08
608.88 4.00 .08 811.96 2.93 .09 810.93 3.19 .08 814.03 2.43 .09 813.00 2.51 .09 814.03 2.41 .09 815.07 2.28 .09 816.10 2.41 .09 817.14 2.72 .09 818.19 2.89 .09 819.23 2.56 .09 820.28 2.54 .09 821.32 2.43 .09 820.28 2.54 .09 821.32 2.43 .09 822.38 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 821.32 2.43 .09 824.48 2.16 .09 821.32 2.43 .09 824.48 2.16 .09 822.38 2.42 .09 824.48 2.16 .09 825.54 1.84 .10 826.60 2.11 .09 827.66 1.77 .10 828.72 1.75 .10 829.78 1.89 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>. U8</td></td<>						. U8
810.93 3.19 .00 814.03 2.43 .09 813.00 2.51 .09 814.03 2.41 .09 815.07 2.28 .09 816.10 2.41 .09 817.14 2.72 .09 818.19 2.89 .09 819.23 2.56 .09 820.28 2.54 .09 821.32 2.43 .09 822.38 2.48 .09 823.43 2.42 .09 824.48 2.16 .09 823.43 2.42 .09 824.48 2.16 .09 825.54 1.84 .10 826.60 2.11 .09 827.66 1.77 .10 826.60 2.11 .09 827.66 1.77 .10 826.72 1.75 .10 829.78 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 837.30 3.11 .10 838.38 3.40 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>.09</td></td<>						.09
813.00 2.51 .09 816.10 2.41 .09 815.07 2.28 .09 816.10 2.41 .09 817.14 2.72 .09 818.19 2.89 .09 819.23 2.56 .09 820.28 2.54 .09 821.32 2.43 .09 822.38 2.48 .09 823.43 2.42 .09 824.48 2.16 .09 823.43 2.42 .09 826.60 2.11 .09 825.54 1.84 .10 826.60 2.11 .09 827.66 1.77 .10 826.72 1.75 .10 829.78 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.30 3.11 .10 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 <td< td=""><td></td><td></td><td>.00</td><td></td><td></td><td>.09</td></td<>			.00			.09
815.07 2.28 .09 818.19 2.89 .09 817.14 2.72 .09 820.28 2.54 .09 819.23 2.56 .09 820.28 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 823.43 2.42 .09 824.48 2.16 .09 825.54 1.84 .10 826.72 1.75 .10 827.66 1.77 .10 826.72 1.75 .10 829.78 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.30 3.11 .10 840.55 3.03 .10 841.63 3.62 .09 840.55 3.03 .10 843.82 3.17 .10 844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>.09</td></td<>						.09
817.14 2.72 .09 820.28 2.54 .09 819.23 2.56 .09 820.28 2.48 .09 821.32 2.43 .09 822.38 2.48 .09 823.43 2.42 .09 824.48 2.16 .09 825.54 1.84 .10 826.60 2.11 .09 827.66 1.77 .10 826.72 1.75 .10 829.78 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.30 3.11 .10 838.38 3.40 .10 839.46 3.62 .09 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 .10 843.82 3.17 .10 847.11 2.80 .10 846.01 2.72 .10 847.11 2.80 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>.09</td></td<>						.09
819.23 2.56 .09 822.38 2.48 .09 821.32 2.43 .09 824.48 2.16 .09 823.43 2.42 .09 824.48 2.16 .09 825.54 1.84 .10 826.60 2.11 .09 827.66 1.77 .10 826.72 1.75 .10 829.78 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.30 3.11 .10 838.38 3.40 .10 839.46 3.62 .09 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 .10 843.82 3.17 .10 844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 <td< td=""><td>817.14</td><td></td><td>.09</td><td></td><td></td><td></td></td<>	817.14		.09			
821.32 2.42 .09 824.48 2.16 .09 825.54 1.84 .10 826.60 2.11 .09 827.66 1.77 .10 826.72 1.75 .10 829.78 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.50 3.11 .10 838.38 3.40 .10 839.46 3.62 .09 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 .10 843.82 3.17 .10 844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11			.09			
823.43 2.42 .00 826.60 2.11 .09 827.66 1.77 .10 826.72 1.75 .10 829.78 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.30 3.11 .10 838.38 3.40 .10 839.46 3.62 .09 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 .10 843.82 3.17 .10 844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11			.09			
825.54 1.84 .10 828.72 1.75 .10 827.66 1.77 .10 828.72 1.75 .10 829.78 1.89 .09 830.85 2.02 .09 831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.30 3.11 .10 838.38 3.40 .10 839.46 3.62 .09 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 .10 843.82 3.17 .10 844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11						
829.78						
831.92 2.09 .09 832.99 1.98 .15 834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.30 3.11 .10 838.38 3.40 .10 839.46 3.62 .09 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 .10 843.82 3.17 .10 844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 .10 848.21 2.72 .10 847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11						
834.06 2.30 .11 835.14 2.44 .11 836.22 2.77 .11 837.30 3.11 .10 838.38 3.40 .10 839.46 3.62 .09 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 .10 843.82 3.17 .10 844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11						
836.22 2.77 .11 837.30 3.11 .10 838.38 3.40 .10 839.46 3.62 .09 840.55 3.03 .10 841.63 3.05 .10 842.72 3.19 .10 843.82 3.17 .10 844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11						
838.38						
840.55	836.22	2,77				
842.72	838.38					
844.91 3.12 .10 846.01 2.72 .10 847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11	840.55					
847.11 2.80 .10 848.21 2.94 .10 849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11	842.72	3,19	.10			
849.31 3.54 .09 850.41 3.70 .09 851.52 3.00 .10 852.63 2.50 .11	844.91	3.12				
851.52 3.00 .10 852.63 2.50 .11	847.11	2,80	.10	848.21		
851.52 3.00 .10 852.63 2.50 .11	849.31	3.54	. 19	850.41		
853.74 1.99 .11 854.86 1.69 .12		3.00	.10	852.63	2.50	
2,017	853.74	1.99	.11	854,86	1.69	.12

E _n , keV	σ _T , b	dσ _T , b	E _n , keV	σ _T , b	dσ _T , b
855.97	1.44	.12	85/.09	1./4	.12
658.21	1.95	.11	859.33	2.60	.10
860.46	2.59	.10	861.59	2.69	.10
862.71	3.21	.10	863.85	3.22	.10
864.98	3.45	.09	666.12	3.75	.09
867.25	3.82	.09	868.40	4.52	.09
869.54	4.95	.08	370.68	4.86	.08
871.83	5.40	.08	372.98	4,92	.08
674.13	4.21	.08	875,29	3.75	.09
876.44	3.46	.09	871,60	3.65	.09
878.76	3.27	.09	879.93	3.40	.09
881.09	3.70	.09	882.26	3.92	.09
883.43	4.30	.08	884.61	4.71	.08
885.78	4.21	.08	886.96	4,21	.08
888.14	3.71	. 09	889.32	3.34	.09
890.51	3.10	. 09	891,69	3,16	.09
892.88	3.17	. 49	894.08	3.03	.09
895.27	3.25	.09	896.47	3.00	.09
897.67	3.10	.09	898.87	2.47	.10
900.07	2.79	.10	901.28	2.73	.10
902.49	3.25	.09	903.70	3.46	.09
904.91	4.00	.08	900.13	4.31	.08
907.35	4.27	.08	908.57	4,21	.08
909.80	3.61	.08	911.02	3.72	.09
912.25	3.17	.09	913.48	3.04	.09
914.72	2.78	.09	910.95	2.59	.10
917.19	2.48	.10	918.43	2,22	.10
919.68	2.59	.10	920.92	3,29	.08
922.17	3.28	. 09	923.43	3.81	.08
924.68	3.69	.08	925.94	4.56	.08
927.20	4.19	.08	928,46	4./1	.08
929.72	4.55	.08	933,53	3.38	.09
932.26	4.11	.08	936.09	3,12	.09
934.81	3.10	.09	930.09	3.13	.09
937.37	3.03	.09	941.23	3.27	.09
939.94	3.10	.09	945.81	3.33	.13
942.52	2.97	.09	946.41	3.34	.09
945.11	3.32		949.01	2.91	.09
947.71	2.87	.09	951.63	2.64	.09
950.32	2.70	.09	954.26	3.01	.09
952.95	2.61	.08	956.90	3.21	.09
955.58	3.43	.09	777,75	2.44	.09
958.23	3.05	. 0 7			

					Ja h
E _n , keV	σ _T , b	$d\sigma_{\mathbf{T}}$, b	E _n , keV	σ _T , b	dσ _T , b
11-			962.21	2.42	.09
960.88	2.59	.09	964.89	2.62	.09
963.55	2,68	.09	968,92	3,90	.08
966.23	3.15	.09	971.62	4.02	.08
970.27	4.26	.07	974.33	3,76	.08
972.97	4.12	.08	977.06	3.26	.09
975.69	2.75	.09	979,19	3.79	.08
978.42	3.44	.08	982.54	3,49	.08
981.16	3.75	.08	985.30	2.83	.09
983.92	3.18	.09	988.07	2.17	.09
986.68	2.77	.09	990.85	2.86	.09
989.46	2.75	.09	993.65	2.95	.09
992.25	2.95	.09	996.45	2,65	.10
995.05	3.05	.09	999,27	3,27	.09
997.86	2.92	.09	1002.10	3.04	.09
1000.69	2.65	.10	1004.95	3.24	.09
1003.52	2.83	.10	1007.80	3,53	.09
1006.37	3,17	.10	1010.67	2.64	.10
1009.23	2.84	.10	1013.55	3.47	.09
1012.11	3.19	.09	1016.44	4.04	.08
1014.99	3.77	. 09	1020,80	3.22	.09
1017.89	3.79	.09	1020.80	3.22	.09
1019.34	3.25	.09	1023,72	2.68	.10
1022.26	2,67	.10	1026.66	2.31	.10
1025.19	2.54	.10	1029.61	2.03	.10
1028.13	2.38	.10	1032.57	2.44	.10
1031.09	2.33	.10	1032.25	2.45	.10
1034.06	2.34	.10	1040.03	2.51	.10
1037.04	2.38	.10	1045.04	2,95	.09
1041.53	2.52 3.09	. 10	1046.06	2.68	.09
1044.55	2.65	.09	1049.09	2,38	.09
1047.58	2.15	.10	1052.14	2.58	.09
1050.62	2.16	.10	1055.20	2.47	.14
1056.74	2.79	.14	1058.28	2.85	.13
1059.82	2.93	.13	1061.36	3.17	.09
1062.91	2.90	.09	1064,46	2.92	.09
1066.02	2.71	.09	106/.08	2.75	.09
1069.14	3.20	.09	1070./1	3.08	.09
1072.28	3.18	.09	1073.85	3.04	.09
1075.43	3.16	.09	107/.01	3.28	.09
1078.59	3.32	.09	1080.18	3.50	.08
1081.77	3.25	.09	1083,36	3,31	.09
1084.96	3.44	.08	1086.56	3,50	.08
1004.70	0,77		1000,00	0,00	• • •

TABLE V (Contd.)

E _n , keV	σ _T , b	dσ _T , b	E _n , keV	σ _T , b	$d\sigma_{\mathbf{T}}$, b
1088.17	3.46	.08	1089.78	3.00	.08
1091.39	3.27	. 49	1093.00	3.47	.08
1094.62	3.31	. 09	1096.25	3,48	.08
1099.50	3.12	.14	1101,14	3.84	.09
1102.77	4.15	.09	1104,41	4,65	.08
1106.06	4.16	.09	1107.71	4,51	.09
1109.36	4.15	. 09	1111.02	3.75	.09
1112.68	3.49	.09	1114.54	5,44	.09
1116.01	3.29	.09	1117.68	3,52	.09
1119.35	3.96	.08	1121.03	4.09	.08
1122.71	4.02	.08	1124.40	3,61	.08
1126.09	3.55	.08	1127.79	3,44	.08
1129.48	3.48	.08	1131,19	3,38	.08
1132.89	3.40	.08	1134.60	2.94	.08
1136.31	3.26	.08	1138.03	3,54	.08
1139.75	4.12	. 07	1141.48	4,51	.07
1143.21	4.10	.07	1144.94	3,32	.08
1146.68	2.64	.08	1148.42	2,59	.08
1150.16	2.65	.08	1151.91	2.82	.08
1153.67	2.87	.08	1155.42	3.34	.07
1157.18	3.53	.07	1158.95	3,79	.07
1160.72	3,35	.07	1162.49	2,97	.08
1164.27	2.79	.08	1166.05	2,93	.08
1167.84	3.05	.08	1169.63	3,72	.07
1171.42	3.61	.07	1173.22	3,89	.07
1175.02	3.49	.07	1176,83	3.87 4.03	.07
1178.64	4.07	.07	1180.45	3,63	.07
1182.27	3.82	.07	1187.76	3,03	.07
1185.92	3.16	.07	1191.43	3.15	.07
1189.59	2.96	.07	1195.13	3,43	.07
1196.98	3.54	.07	1198.84	3,60	.07
1200.70	3.06	.07	1202.57	3,13	.07
1204.44	3.30	.07	1206.31	3,46	.07
1208.19	2.98	.07	1210.08	2,89	.07
1211.97	2.67	.08	1213.86	2.64	.07
1215.76	2.47	.08	1217.66	2,75	.07
1219.57	3.23	.07	1221.48	3,14	.07
1223.39	3.30	.07	1225,31	3,53	.07
1227.24	3.44	. 17	1229.17	3,75	.06
1231.10	3.51	.07	1233.04	2,88	.07
1234.98	2.68	.12	1236.93	3,25	.08
1238.88	3,54	. U8	1240.84	3,60	.08

E _n , keV	σ _T , b	dσ _T , b	E _n , keV	σ _T , b	dσ _T , b
			1244./7	3,95	.07
1242.80	3.84	.07		3.92	.07
1246.74	3,97	. 07	1248./1	3,65	.08
1250.69	3.67	.07	1252.68	3.02	.08
1254.67	3.34	.08	1256.67	2,35	.09
1258.66	2.71	.08	1260.67	2.65	.08
1262.68	2.40	.09	1264.69	2.64	.08
1266.71	2,68	. u8	1268.74	3.05	.08
1270.76	3.17	. U8	1272.80	2.73	.08
1274.84	3.04	.08	1276.88	2.81	.08
1278.93	2.72	. U8	1280.98	3.23	.08
1283.04	2.83	.08	1285.10	3,40	.08
1287.17	3.58	. U8	1289,25	3,09	.08
1291.32	3.32	.08	1293,41	3,23	.08
1295.50	3.12	.08	1297.59	3,75	.07
1299.69	3.18	.08	1301.79		.07
1303.90	3.77	.07	1306.02	3.97	.08
1308.14	3.75	. 07	1310.26	3,60	
1312.39	3.54	.08	1314.53	3,32	.08
1316.67	3.21	.08	1318.81	3.43	.08
1320.96	3.76	.07	1323,12	4.05	.07
1325.28	3.90	.07	1321,45	3.90	.07
1329.62	3.77	.07	1531.80	3./2	.07
1333.98	3.49	.08	1536.17	3.18	.08
1338.36	3.39	.08	1540,56	3.48	.08
1342.77	3.47	.11	1344.98	3,53	.11
1347.19	3.40	.07	1349,42	3.44	.07
1351.64	3.08	.07	1353.88	2,96	.07
1356.11	2,68	.07	1358.36	2.90	.07
1360.61	2.92	. 07	1362.86	2.91	.07
1365.12	3.29	.06	1367.39	3,23	.07
1369.66	3.05	. 17	1571.94	3.49	.06
1374.22	3.15	. 47	1370.51	2.87	.07
1378.80	2.86	.07	1381.10	2,68	.07
1383.41	2.90	.07	1385,72	2,93	.06
1388.04	2.98	.06	1390.36	5.05	.06
1392.69	3.14	.06	1595.03	3,16	.06
1397.37	3.21	.06	1399,72	3,50	.06
1402.07	3.45	.06	1404.43	3.41	.06
1406.80	3,30	.06	1409.17	3,44	.06
1411.55	3.16	. 46	1415.93	3,26	.06
1416.32	3.00	.06	1418./1	3,12	.06
1421.12	3.23	.06	1423.52	3,25	.06
1425.94	3.47	.05	1428.36	3.63	.05
1430.79	4.20	.05	1433,22	4,15	.05
1435.66	4.05	.05	1438.10	4.38	.05
1402.00	4,00				

TABLE VI. Differential Elastic Scattering Cross Sections of Vanadium, Expressed in Format of Eq. 1

E _n , keV	σ _{el} , b	ω_1	$d\omega_1$	ω ₂	dω ₂	ω_3	dw3	ω4	$d\omega_4$
326.00	4.720	.3550	. 0300	.1270	.0440	.0880	. 0550	0250	. 0740
329.00	4.750	.3300	.0300	.1>30	.0450	.0870	. 0560	0240	. 0760
337.00	4.560	.3800	.0310	.142U	. 0470	.0770	. 0580	0150	. 0790
345.00	4.440	.3820	.0360	.1420	. 0530	.0510	. 0660	0040	. 0890
347.00	4.360	.3990	.0340	.1420	.0510	.0610	.0630	.0060	.0850
355.00	4.210	.4080	. 0340	.1570	.0510	.0230	. 0630	0200	.0860
357.00	4.130	.4200	. 0340	.1520	.0510	.0230	. 0630	0040	. 4850
365.00	3.970	.4520	.0320	.1700	.0480	.0190	.0600	.0010	.0800
367.00	3.930	.4550	.0330	.1720	.0500	0020	.0620	0000	. 0830
375.00	3.760	.4220	.0330	.1350	.0490	0090	. 0610	0250	.0820
377.00	3.650	.4300	.0340	.1900	.0510	0160	. 4640	0200	. 0860
385.00	3.580	.4320	. 0360	.2040	.0530	.0040	. 4660	.0090	.0890
387.00	3.570	.4320	. U 3 4 U	.2300	.0510	.0070	. 0630	.0250	. 0850
392.00	3.540	.4280	. 0340	.2540	.0500	.0020	. 0620	.0240	. 0840
395.00	3.550	.4390	.0310	.2300	.0460	.0150	.0580	.0390	. 4770
403.00	3.450	.4400	.0290	.2700	.0440	.0030	. 0550	. 0300	.0730
406.00	3.390	.4380	.0310	.2740	.0470	.0180	. 0580	. 0340	.0780
414.00	3.370	.4250	. 0300	.3130	.0450	.0390	. 0560	. 0540	. 0750
417.00	3.370	.4210	.0310	.3040	.0460	.0310	.0570	.0600	.0770
425.00	3.380	.4020	.0280	.2970	.0420	.0280	. 0520	.0380	.0710
428.00	3.380	.4120	.0280	.3080	.0420	.0400	. 0530	.0550	. 0710
436.00	3.490	.4140	.0280	.3210	.0420	.0450	.0520	.0450	.0710
439.00	3.500	.4150	.0260	.3300	.0380	.0430	. 0480	.0390	. 0650
447.00	3.570	.42/0	.0250	.3240	.0380	.0420	. 0470	.0250	.0630
455.00	3.580	.4540	.0260	.3180	.0380	.0410	. 4/0	.0210	. 0640
457.00	3.590	.4300	.0270	.3270	. 400	.0430	.0500	.0190	.0670
465.00	3.580	.4510	.0250	.3180	.0380	.0330	. 4/0	.0210	. 0630
467.00	3.610	.45/0	.0250	.3120	.0380	.0320	. 0470	.0220	. 0630
475.00	3.540	.4930	.0240	.3180	.0350	.0380	. 0440	.0120	.0590
477.00	3.550	.5060	. 0240	.3170	.0350	.0410	. 0440	.0250	. 0590
485.00	3.450	.52/0	.0220	.3340	.0330	.0430	.0410	.0190	. 0550
487.00	3.400	.5410	.0210	.3280	.0320	.0410	. 4400	.0200	.0530
495.00	3.360	.5200	.0200	.3410	.0300	.0360	.0380	. 0240	.0510
497.00	3.320	.55/0	.0190	.3400	.0290	.0300	.0360	.0180	. 0490
505.00	3.250	.5750	.0190	.3590	.0280	.0320	. 0350	.0300	.0470
507.00	3.210	.5830	.0190	.3530	.0290	.0350	.0360	.0330	.0480
515.00	3.170	.58/0	.0210	.4010	.0320	.0550	.0390	.0530	. 0530
517.00	3.100	.5910	.0210	.4120	.0310	.0690	. 0390	.0600	. 0530
525.00	3.050	.5800	.0200	.4450	.0300	.0730	. 03/0	.0520	.0500
527.00	3.040	.5/10	.0<00	.4470	.0300	.0710	.0370	.0480	.0500

TABLE VI (Contd.)

									dw4
En, keV	σ _{el} , b	ω_1	$d\omega_1$	ωz	dωz	ω3	$d\omega_3$	ω4	d ω4
532.00	3.000	.5730	.0210	.4550	.0310	.0700	. 0390	.0460	.0520
535.00	2.990	.5750	.0210	.4720	.0320	.0770	.0400	.0510	.0540
541.00	2.950	.5500	.0200	.4850	.0300	.0930	. 03/0	.0570	.0500
543.00	2.900	.5500	.0210	.5010	.0310	.1080	. 0390	.0610	.0530
553.00	2.810	.4690	.0220	.4970	.0330	.1030	. 0410	.0340	.0550
555.00	2.770	.4480	.0240	.5060	.0350	.1040	. 440	.0320	.0590
565.00	2.810	.3730	.0210	.5080	.0320	.1070	.0400	.0300	. 0540
567.00	2./80	.3490	.0210	.5090	.0310	.0970	.0390	.0140	.0530
577.00	2.870	.30/0	.0200	.4920	.0300	.0860	.03/0	.0110	.0490
580.00	2.890	.2820	.0200	.4900	.0300	.0880	.0380	.0070	.0510
589.00	3.000	.2790	.0200	.4780	.0290	.0970	. 03/0	.0130	0490
597.00	3.070	.2920	.0200	.4650	.0300	.1040	.0370	.0180	.0500
605.00	3.070	.3130	.0200	.4540	.0300	.0810	. 03/0	.0170	.0490
607.00	3.110	.3260	.0190	.4630	.0290	.0870	. 0360	.0230	.0490
615.00	3.140	.3410	.0190	.4/60	.0280	.0590	.0350	.0240	.0470
617.00	3.150	.3590	.0190	.4730	.0290	.0530	.0360	.0180	.0480
	3.150	.3590	.0180	.4830	.0280	.0350	. 0350	.0150	.0470
625.00 627.00	3.120	.3700	.0180	.4830	.0270	.0330	. 0340	.0080	.0450
	3.200	.3610	.0180	.4920	.0270	.0330	. 0330	.0130	.0450
635.00	3.190	.3620	.0180	.4960	.0260	.0210	. 0330	.0050	. 440
	3.240	.3470	.0180	.5140	.0260	.0320	. 0350	.0200	. 0440
645.00	3.240	.3360	.0160	.5180	.0240	.0240	.0300	.0150	.0410
647.00	3.270	.3120	.0160	.5370	.0240	.0440	.0290	.0310	. 0400
655.00	3.310	.3040	.0150	.5430	.0230	.0510	. 0290	.0360	.0390
657.00	3.340	.3020	.0160	.5500	.0240	.0510	.0300	. 0300	.0410
665.00	3.350	.3010	0150	.5520	.0220	.0610	.0280	.0260	.0380
667.00		.30/0	.0160	.5400	.0240	.0780	. 0300	.0250	.0410
675.00	3.370	.3090	.0170	.5480	.0260	.0940	.0320	. 0320	. 440
677.00	3.400	.3360	0180	.5320	.0280	.1040	.0340	.0320	. 0470
685.00	3.450		0190	.5330	.0280	.1160	.0350	.0360	. 470
687.00	3,420	.3450	.0180	.5230	.0270	.1130	. 0340	.0220	. 0450
695.00	3.430	.3660	.0190	.5160	.0280	.1150	. 0350	.0180	. 0470
697.00	3.410	.37/0	.0180	.5090	.0280	.1070	. U340	0010	.0470
705.00	3.430	.3900	.0190	.5010	.0290	.1010	. 0360	0150	.0480
707.00	3.430	.4030		.5120	.0300	.0900	. 0370	0200	.0500
715.00	3.440	.4350	.0200	.5000	.0300	.0960	. 0380	0270	.0510
717.00	3.450	.4490	.0200	.5170	.0320	.1010	.0400	00>0	. 0540
725.00	3.400	.4850	.0220	.5200	. 0330	.1020	.0410	0070	.0550
727.00	3.410	.5030	.0220		.0360	.1000	.0450	.0090	.0610
735.00	3.300	.5390	.0240	.5570	.0350	.1000	. 0440	.0090	.0590
737.00	3.260	.5550	.0240	.5750	.0400	.0820	.0500	0030	.0670
745.00	3.080	.5530	.0270	.5970	.0400	.0850	.0520	.0020	.0700
747.00	3.030	.5650	.0280	.6150	.0380	• 0730	. 0480	.0060	.0640
755.00	2.940	.5430	.0260	.6370	.0380	.0/30	, 3 , 0 0	. , , , ,	

TABLE IV (Contd.)

$\begin{array}{cccccccccccccccccccccccccccccccccccc$. U500 . U480 . U470 . U490 . U490 . U490 . U490 . U460 . U480 .	0110
765.00	. U 480	01>0
765.00 2.800 .5340 .0260 .6510 .0390 .0710 767.00 2.710 .5400 .0250 .6560 .0380 .0740 775.00 2.670 .4930 .0260 .6810 .0390 .0680 777.00 2.610 .4820 .0270 .6930 .0400 .0610 785.00 2.610 .4390 .0260 .7010 .0390 .0670 787.00 2.590 .4180 .0250 .7060 .0370 .0600 795.00 2.640 .3780 .0250 .6780 .0470 .0700 797.00 2.650 .3620 .0270 .7000 .0400 .0800 808.00 2.670 .3520 .0220 .7100 .0330 .1000 820.00 2.670 .3260 .0250 .7350 .0370 .1300 822.00 2.660 .3190 .0250 .7350 .0370 .1390 828.00 2.720 <td>. 0 4 7 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0</td> <td>0230</td>	. 0 4 7 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0	0230
767.00	. 0 4 9 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0	0360
775.00	.0490 .0 .0490 .0 .0460 .0 .0460 .0 .0490 .0 .0490 .0 .0460 .0 .0 .0460 .0 .0 .0460 .0 .0 .0460 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .	0340
777.00	.0490 .0 .0460 .0 .0490 .0 .0490 .0 .0430 .0 .0460 .0 .0460 .0 .0460 .0 .0460 .0 .0460 .0 .0460 .0 .0460 .0 .0460 .0 .0480 .0 .0480 .0	0240
785.00	. U 460 . 0 . U 460 . 0 . U 420 . 0 . U 420 . 0 . U 460 . 0	0190
787.00	.0460 .0 .0490 .0 .0420 .0 .0430 .0 .0460 .0 .0460 .0 .0460 .0 .0460 .0 .0460 .0 .0460 .0 .0480 .0 .0480 .0	0300
795.00	.0490 .0420 .0020	02>0
797.00 2.650 .3620 .0270 .7000 .0400 .0800 808.00 2.670 .3520 .0220 .7100 .0330 .1000 810.00 2.670 .3260 .0230 .7080 .0340 .1070 820.00 2.660 .3190 .0250 .7350 .0370 .1300 828.00 2.720 .3010 .0250 .7500 .0370 .1390 830.00 2.730 .3000 .0250 .7500 .0370 .1440 838.00 2.720 .3030 .0250 .7750 .0380 .1670 844.00 2.710 .3060 .0250 .7750 .0380 .1670 844.00 2.720 .3030 .0250 .7750 .0380 .1670 844.00 2.770 .2860 .0260 .7870 .0390 .1710 846.00 2.730 .2600 .0260 .7890 .0390 .1710 851.00 2.7740 </td <td>.0420 .0 .0430 .0 .0460 .0 .0460 .0 .0450 .0 .0470 .0 .0480 .0</td> <td>0390 .0560 0460 .0570 0690 .0630 0740 .0620 0700 .0620 0820 .0630 0820 .0630 0930 .0650</td>	.0420 .0 .0430 .0 .0460 .0 .0460 .0 .0450 .0 .0470 .0 .0480 .0	0390 .0560 0460 .0570 0690 .0630 0740 .0620 0700 .0620 0820 .0630 0820 .0630 0930 .0650
808.00 2.670 .3520 .0220 .7100 .0330 .1000 810.00 2.670 .3500 .0230 .7080 .0340 .1070 820.00 2.670 .3260 .0250 .7350 .0370 .13300 822.00 2.660 .3190 .0250 .7450 .0370 .1320 828.00 2.720 .3010 .0250 .7570 .0370 .1320 830.00 2.730 .3010 .0250 .7500 .0370 .1390 840.00 2.710 .3050 .0250 .7750 .0380 .1650 844.00 2.710 .3060 .0250 .7750 .0380 .1650 844.00 2.710 .3060 .0260 .7260 .0390 .1680 844.00 2.720 .2860 .0260 .7890 .0390 .1710 844.00 2.730 .2600 .0260 .7890 .0390 .1710 851.00 2.730 </td <td>. 0 4 3 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0</td> <td>0460 .0570 0690 .0630 0740 .0620 0700 .0620 0670 .0620 0860 .0630 0860 .0630 0930 .0650</td>	. 0 4 3 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0	0460 .0570 0690 .0630 0740 .0620 0700 .0620 0670 .0620 0860 .0630 0860 .0630 0930 .0650
810.00 2.670 .3500 .0230 .7080 .0340 .1070 820.00 2.670 .3260 .0250 .7350 .0370 .1320 822.00 2.660 .3190 .0250 .7450 .0370 .1320 828.00 2.720 .3010 .0250 .7570 .0370 .1390 830.00 2.730 .3000 .0250 .7750 .0380 .1650 840.00 2.710 .3030 .0250 .7750 .0380 .1650 844.00 2.710 .3040 .0250 .7750 .0380 .1670 844.00 2.720 .2800 .0260 .7870 .0390 .1680 844.00 2.730 .2600 .0260 .7890 .0390 .1710 851.00 2.730 .2600 .0270 .7380 .0400 .1630 852.00 2.740 .2500 .0270 .7380 .0400 .1630 853.00 2.740 <td>.0460 .0 .0460 .0 .0460 .0 .0450 .0 .0470 .0 .0460 .0</td> <td>0690 10630 0740 10620 0740 10620 0670 10620 0820 10630 0840 10630</td>	.0460 .0 .0460 .0 .0460 .0 .0450 .0 .0470 .0 .0460 .0	0690 10630 0740 10620 0740 10620 0670 10620 0820 10630 0840 10630
820.00 2.670 .3260 .0250 .7350 .0370 .1300 822.00 2.660 .3190 .0250 .7450 .0370 .1320 828.00 2.720 .3010 .0250 .7500 .0370 .1390 830.00 2.720 .3030 .0250 .7500 .0370 .1440 838.00 2.720 .3030 .0250 .7750 .0380 .1670 844.00 2.720 .2800 .0250 .7750 .0380 .1670 844.00 2.720 .2800 .0260 .7590 .0390 .1680 846.00 2.700 .2910 .0260 .7980 .0390 .1710 851.00 2.730 .2600 .0270 .7980 .0400 .1630 852.00 2.740 .2460 .0270 .7980 .0400 .1610 853.00 2.740 .2460 .0270 .7990 .0400 .1640 855.00 2.750 <td>. U 46 0 . U 45 0 . U 45 0 . U 46 0 . U 48 0 . U</td> <td>0740 .0620 0740 .0620 0670 .0620 0820 .0630 0880 .0630</td>	. U 46 0 . U 45 0 . U 45 0 . U 46 0 . U 48 0 . U	0740 .0620 0740 .0620 0670 .0620 0820 .0630 0880 .0630
822.00 2.660 .3190 .0250 .7450 .0370 .1320 828.00 2.720 .3010 .0250 .7570 .0370 .1390 830.00 2.730 .3000 .0250 .7500 .0370 .1440 838.00 2.720 .3030 .0250 .7750 .0380 .1650 844.00 2.710 .3060 .0250 .7750 .0380 .1650 844.00 2.720 .2860 .0260 .7890 .0390 .1710 846.00 2.730 .2600 .0270 .7890 .0390 .1710 851.00 2.730 .2600 .0270 .7890 .0490 .1610 853.00 2.740 .2550 .0270 .8020 .0400 .1610 853.00 2.740 .2460 .0270 .8020 .0400 .1610 855.00 2.750 .2410 .0270 .8040 .0410 .1640 855.00 2.850 <td>.0460 .0 .0450 .0 .0470 .0 .0460 .0 .0480 .0</td> <td>0700 .0620 0670 .0620 0820 .0630 0860 .0630 0930 .0650</td>	.0460 .0 .0450 .0 .0470 .0 .0460 .0 .0480 .0	0700 .0620 0670 .0620 0820 .0630 0860 .0630 0930 .0650
828.00 2.720 .3010 .0250 .7270 .0370 .1390 830.00 2.730 .3000 .0250 .7500 .0370 .1440 838.00 2.720 .3030 .0250 .7750 .0380 .1650 840.00 2.710 .3040 .0250 .7750 .0380 .1670 844.00 2.720 .2860 .0260 .0260 .0390 .1680 846.00 2.700 .2910 .0260 .7890 .0390 .1710 851.00 2.730 .2600 .0270 .7890 .0400 .1630 852.00 2.740 .2500 .0270 .8020 .0400 .1610 853.00 2.740 .2460 .0270 .8020 .0400 .1640 855.00 2.750 .2410 .0270 .8040 .0410 .1630 860.00 2.840 .2070 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0290 .8090 .0430 .1480 865.00	.U450 .U .U470 .U .U460 .U .U480 .U	0670 .0620 0820 .0630 0860 .0630 0930 .0650
830.00 2.730 .3000 .0250 .7500 .0370 .1440 838.00 2.720 .3030 .0250 .7750 .0380 .1650 840.00 2.710 .3060 .0250 .7750 .0380 .1670 844.00 2.720 .2860 .0260 .7870 .0390 .1680 846.00 2.730 .2600 .0240 .7890 .0490 .1710 851.00 2.730 .2600 .0270 .7980 .0400 .1630 852.00 2.740 .2550 .0270 .7990 .0400 .1610 853.00 2.740 .2460 .0270 .7990 .0400 .1640 855.00 2.750 .2410 .0270 .8040 .0410 .1630 860.00 2.830 .2150 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0280 .8090 .0430 .1480 865.00 2.850 .2050 .0290 .8020 .0430 .1490 871.00	.U460 .U .U460 .U .U480 .U	0820 .U630 0860 .U630 0930 .U650
838.00 2.720 .30.50 .0250 .7750 .0380 .1650 840.00 2.710 .30.60 .0250 .7750 .0380 .1650 844.00 2.720 .2860 .0260 .7870 .0390 .1680 846.00 2.700 .2910 .0260 .7890 .0390 .1710 851.00 2.730 .2600 .0270 .0390 .0400 .1630 852.00 2.740 .2550 .0270 .8020 .0400 .1610 853.00 2.740 .2460 .0270 .8020 .0400 .16610 855.00 2.750 .2410 .0270 .8040 .0410 .1640 855.00 2.750 .2410 .0270 .8040 .0410 .1630 860.00 2.830 .2130 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0280 .8070 .0420 .1520 863.00 2.850 .2050 .0290 .8020 .0430 .1480 863.00 2.850 .2050 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1490 871.00 2.940 .1840 .0240 .0430 .1490	.U460 .U .U460 .U .U480 .U	0820 .U630 0860 .0630 0930 .U650
840.00 2.710 .3060 .0250 .7750 .0380 .1670 844.00 2.720 .2860 .0260 .7870 .0390 .1680 846.00 2.700 .2910 .0260 .7890 .0390 .1710 851.00 2.730 .2600 .0270 .8020 .0400 .1630 852.00 2.740 .2550 .0270 .8020 .0400 .1610 853.00 2.740 .2460 .0270 .8040 .0410 .1640 855.00 2.750 .2410 .0270 .8040 .0410 .1630 860.00 2.830 .2150 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0290 .8090 .0430 .1480 863.00 2.850 .2050 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1490 871.00 2.940 .1870 .0280 .7880 .0430 .1490 871.00	.U460 .0 .U480 .0	0860 .0630 0930 .0650
844.00 2.720 .2860 .0260 .7870 .0390 .1680 846.00 2.700 .2910 .0260 .7890 .0390 .1710 851.00 2.730 .2600 .0270 .7980 .0400 .1630 852.00 2.740 .2550 .0270 .8020 .0400 .1610 853.00 2.740 .2480 .0270 .7990 .0400 .1640 855.00 2.750 .2410 .0270 .8040 .0410 .1630 860.00 2.830 .2130 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0290 .8090 .0430 .1480 863.00 2.850 .2030 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1490 871.00 2.940 .1840 .0280 .7780 .0410 .1220	. 0480 . 0	
846.00 2.700 .2910 .0260 .7890 .0390 .1710 851.00 2.730 .2600 .0270 .0400 .1630 852.00 2.740 .2550 .0270 .8020 .0400 .16610 853.00 2.740 .2460 .0270 .7990 .0400 .1640 855.00 2.750 .2410 .0270 .8040 .0410 .1630 860.00 2.830 .2130 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0280 .8090 .0430 .1480 863.00 2.850 .2050 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1490 871.00 2.940 .1840 .0280 .7980 .0430 .1490		1910 .0660
851.00 2.730 .2600 .0270 .7780 .0400 .1630 852.00 2.740 .2550 .0270 .8020 .0400 .1610 853.00 2.740 .2400 .0270 .7790 .0400 .1640 855.00 2.750 .2410 .0270 .8040 .0410 .1630 860.00 2.830 .2130 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0290 .8090 .0430 .1480 863.00 2.850 .2030 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1490 871.00 2.940 .1870 .0280 .7780 .0410 .1220		
852.00 2.740 .2500 _U2/U .802U .040U .1610 853.00 2.740 .2400 .U2/U .7990 .U40U .1640 855.00 2.750 .2410 _U2/U .8040 .U41U .1630 860.00 2.830 .2130 .U28U .807U .042U .1520 861.00 2.84U .2U/O _U29U .809U .U43U .1530 863.00 2.850 .2U30 .U29U .802U .U43U .1530 865.00 2.860 .1980 .U29U .804U .043U .1530 871.00 2.940 .1840 .U29U .798U .U41U .1220	.0490 .0	0920 .0660
853.00 2.740 .2460 _U2/U .7790 .U40U .1640 855.00 2.750 .2410 .U2/U .8040 .U41U .1630 860.00 2.830 .2130 .U28U .807U .042U .1520 861.00 2.84U .2U/O .U29U .8090 .U43U .1480 863.00 2.850 .2U30 .U29U .802U .U43U .1530 865.00 2.860 .1980 .U29U .804U .U43U .1490 871.00 2.940 .1840 .U28U .778U .U41U .1220		0930 .0670
855.00 2.750 .2410 .0270 .8040 .0410 .1630 860.00 2.830 .2130 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0290 .8090 .0430 .1480 863.00 2.850 .2030 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1530 871.00 2.940 .1870 .0280 .7980 .0410 .1220		0950 .0660
860.00 2.830 .2130 .0280 .8070 .0420 .1520 861.00 2.840 .2070 .0290 .8090 .0430 .1480 863.00 2.850 .2030 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1530 871.00 2.940 .1890 .0280 .7980 .0410 .1220	.0500 .0	0970 .0680
861.00 2.840 .20/0 _0290 .8090 .0430 .1480 863.00 2.850 .20>0 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1490 871.00 2.940 .1890 .0280 .7980 .0410 .1220	.0520 .0	0880 .0710
863.00 2.850 .2050 .0290 .8020 .0430 .1530 865.00 2.860 .1980 .0290 .8040 .0430 .1490 871.00 2.940 .1890 .0280 .7980 .0410 .1220	.0520 .0	0840 .0710
871.00 2.940 .1870 .0280 .7780 .0410 .1220	. 0530 .0	0780 .0720
871.00 2.940 .1870 .0280 .7780 .0410 .1220	. 0530 .0	0730 .0720
	.0510 .0	0690
872.00 2.940 .1930 .02/0 .7990 .0400 .1220	.0500 .0	0670
874.00 2.940 .18/0 .0280 .8030 .0420 .1190	.0520 .0	0700 .0700
881.00 3.020 .1910 .0290 .7970 .0440 .1110	. 0540 . 0	0840 .0730
883.00 3.040 .19.0 .0300 .7920 .0450 .1130	. 0560 .0	0820 .0760
885.00 3.070 .17/0 .0300 .7910 .0450 .0980		0730 .0740
887.00 3.120 .1600 .0290 .7890 .0440 .0800	.0540 .0	0620 .0730
895.00 3.240 .1600 .0300 .7520 .0450 .0660		0530 .0750
897.00 3.260 .1/60 .0290 .7590 .0430 .0690		1520 .0730
905.00 3.390 .2020 .0270 .7380 .0400 .0480		0500 .0670
907.00 3.390 .21-0 .0280 .7580 .0420 .0580		0500 .0700
915.00 3.480 .2640 .0260 .7550 .0390 .0540		.0650
917.00 3.440 .2830 .0230 .7600 .0350 .0600		1780 .0590
925.00 3.500 .3550 .0260 .7300 .0400 .0720	. 4490 .1	.000 .0660
927.00 3.460 .3540 .0260 .7830 .0390 .0820		.010 .0650
935.00 3.480 .39:0 .0260 .8170 .0390 .0910	.0480 .1	.0660

TABLE IV (Contd.)

937.00	E _n , keV	σ _{el} , b	ω_1	$d\omega_1$	ω ₂	$d\omega_2$	ω3	$d\omega_3$	ω4	dω₄
045 00 3 360 4360 10280 8520 0410 0930 1050 1090 1090 0660 947 00 3 360 4420 10260 8520 0410 0930 1090 1090 10660 955 00 3 310 460 10280 8770 0470 1095 0660 1400 1990 10600 1400 10810 955 00 3 300 4770 10320 8770 0470 1095 0660 1400 1990 10600 1400 10810 955 00 3 320 5000 10260 9240 0540 1190 10600 1400 1990 967 00 3 200 5000 10260 9240 0560 1190 10600 1400 1990 967 00 3 200 5000 10260 9240 10560 1190 10600 1400 1990 977 100 3 120 5200 10360 9440 10560 1210 10690 1120 19930 977 100 3 100 5200 10370 9880 10560 1190 10600 1100 10870 987 103 3 000 5200 10370 9880 10560 1210 10600 1190 10870 987 103 3 000 5200 10370 9820 0520 1360 10600 1190 10870 987 103 3 010 5540 10360 9820 0520 1360 10600 1190 10870 10950 997 103 3 010 5540 10360 9980 0520 1360 10600 1190 10870 10950 1007 1007 1007 1007 1007 1007 1007 10	037 00	3 460	3800	.0250	. 8230	.0380	.0940	.04/0	.1230	
947.00 3.860 .4320 .0220 .8520 .0400 .0930 .0490 .1920 .0560 .9790 .955.00 3.310 .4600 .0320 .8770 .0470 .0950 .0590 .1320 .9779 .0950.00 3.300 .4720 .0320 .8970 .0490 .1090 .0500 .1400 .0810 .9600 .9790								.0510	.1030	
0.00								. 0490	.1090	
957.00								. 0590	.1320	
965.00 3.230 .5000 1.0360 .9240 .0560 .1190 .0670 .1390 .0930 967.00 3.200 .5000 .0340 .9230 .0560 .1190 .0690 .1350 .0930 975.00 3.120 .5210 .0380 .9940 .0560 .1210 .0690 .1270 .0930 977.00 3.090 .5220 .0340 .9860 .0550 .1240 .0680 .1180 .0910 985.00 3.040 .5360 .0350 .9980 .0520 .1360 .0650 .1190 .0970 987.00 3.010 .5340 .0360 .9920 .0540 .1390 .0670 .1240 .0980 .0990 .0995.00 3.010 .5340 .0360 .9920 .0540 .1390 .0670 .1240 .0990 .0995.00 3.010 .5540 .0370 .9970 .0550 .1240 .0680 .1120 .0920 .997.00 3.000 .5520 .0370 .9980 .0540 .1390 .0670 .1280 .09910 .1007.00 3.000 .5520 .0370 .9980 .0540 .1200 .0660 .1200 .09910 .1007.00 3.000 .5520 .0370 .9980 .0540 .2060 .0670 .1280 .09910 .1007.00 3.020 .5560 .0350 .9940 .0550 .1220 .0680 .1200 .09910 .1007.00 3.020 .5560 .0350 .9940 .0520 .2130 .0660 .1160 .0870 .1015.00 .2,960 .5990 .0370 .1015.00 .0550 .2350 .0680 .1080 .09920 .117.00 .2,960 .5990 .0370 .1015.00 .0550 .2350 .0680 .1080 .09920 .1017.00 .2,960 .5990 .0380 .10380 .0550 .2350 .0680 .1080 .09920 .1037.00 .2,860 .5990 .0360 .10380 .0550 .2560 .0680 .1080 .09920 .1037.00 .2,860 .5990 .0360 .10380 .0530 .2770 .0860 .1130 .09900 .1037.00 .2,800 .5990 .10350 .10380 .0530 .2770 .0860 .1120 .09900 .1037.00 .2,800 .5990 .10350 .10380 .0530 .2770 .0860 .1120 .0980 .1037.00 .2,960 .5990 .10350 .10380 .0530 .2770 .0860 .1120 .0870 .10370 .2790 .5990 .10350 .10380 .0530 .2770 .0860 .1120 .0870 .108								.0600	.1400	
967.00 3.200 5000 .0300 .9230 .0560 .1190 .0690 .1350 .0930 975.00 3.120 .5200 .0380 .9540 .0560 .1210 .0690 .1270 .0930 977.00 3.090 .5230 .0370 .9880 .0550 .1240 .0680 .1180 .09710 985.00 3.040 .5360 .0350 .9920 .0520 .1360 .0650 .1190 .0870 997.00 3.010 .5340 .0360 .9920 .0540 .1330 .0670 .1080 .0990 995.00 3.010 .5340 .0360 .9920 .0540 .1330 .0670 .1080 .0990 995.00 3.010 .5520 .0370 .9970 .0550 .1710 .0660 .1120 .09910 1005.00 3.040 .5500 .0370 .9980 .0540 .2060 .0670 .1260 .09910 1007.00 3.020 .5660 .0350 .9980 .0540 .2060 .0670 .1260 .09910 1007.00 3.020 .5660 .0350 .9980 .0540 .2060 .0670 .1260 .09910 1017.00 3.020 .5660 .0350 .9980 .0540 .2060 .0670 .1260 .09910 1017.00 2.930 .5990 .0360 .0980 .0550 .2360 .0680 .1080 .09920 1017.00 .2.930 .5990 .0360 .0360 .0550 .2360 .0680 .1080 .09920 1017.00 .2.930 .5990 .0360 .10100 .0550 .2360 .0680 .1080 .09920 1025.00 2.860 .5960 .0360 .10360 .0540 .2610 .0670 .1100 .09940 1027.00 2.860 .5960 .0360 .10360 .0540 .2610 .0670 .1100 .09940 1027.00 2.860 .5960 .0360 .10360 .0550 .2360 .0680 .1080 .09920 1037.00 2.860 .5960 .0360 .10360 .0550 .2800 .0560 .1130 .0890 1037.00 2.790 .5950 .0350 .10350 .0520 .2880 .0550 .1330 .0890 .1020 .0550 .2800 .0550 .1120 .0870 1037.00 2.790 .5950 .0360 .10360 .0550 .2800 .0550 .1120 .0870 1037.00 2.790 .5950 .0350 .10390 .0520 .2840 .0660 .1130 .0880 .1140 .0950 .2920 .0660 .1170 .0920 .10660 .1170 .0920 .10660 .1170 .0920 .10660 .1170 .0920 .10660 .1170 .0920 .10660 .1170 .0920 .10660 .1170 .0920 .10660 .1170 .0920 .10660 .1170 .1070 .0920 .10660 .1060 .1060 .0830 .0690 .1090 .1090 .10660 .1060 .0830 .0690 .1090 .1090 .10660 .1060 .0830 .0690 .1090 .1090 .10660 .1060 .0830 .0690 .1090 .1090 .10660 .1060 .0830 .0690 .1090 .10660 .1060 .1								. 06/0	.1390	
975.00 3.120 5200 10360 .9940 10560 .1210 10690 11270 10930 977.00 3.090 5230 .0370 .9880 .0550 11240 .0880 1180 .0910 985.00 3.040 .5360 .0350 .9920 .0520 .1360 .0650 .1190 .0870 987.00 3.010 .5340 .0350 .9920 .0540 .1390 .0670 .1080 .0900 995.00 3.010 .5520 .0370 .9970 .0550 .1710 .0680 .1120 .0920 997.00 3.000 .5550 .0370 .9970 .0550 .1710 .0680 .1200 .0910 1005.00 3.040 .5550 .0370 .9980 .0540 .2080 .0670 .1260 .0910 1007.00 3.020 .5660 .0350 .9980 .0540 .2080 .0670 .1260 .0910 1015.00 2.960 .5940 .0370 10190 .0550 .2920 .0880 .1200 .0910 1015.00 2.960 .5940 .0370 10190 .0550 .2920 .0880 .1080 .0920 1017.00 2.930 .5940 .0350 .9940 .0520 .2130 .0650 .1080 .0920 1017.00 2.930 .5940 .0360 .0340 .0550 .2360 .0680 .1080 .0920 1017.00 2.930 .5940 .0360 .0360 .0540 .2610 .0670 .1060 .0940 1025.00 2.880 .5940 .0360 .1050 .0540 .2610 .0670 .1060 .0940 1025.00 2.880 .5940 .0360 .1050 .0540 .2610 .0670 .1060 .0940 1025.00 2.880 .5940 .0360 .10380 .0530 .2770 .0660 .1130 .0890 1037.00 2.900 .5950 .0350 .10390 .0520 .2880 .0660 .1130 .0890 1037.00 2.900 .5950 .0350 .10390 .0520 .2880 .0660 .1130 .0890 1035.00 2.800 .5940 .035							.1190	. 4690	.1350	
977.00							.1210	. 0690	.12/0	
985.00						.0550	.1240	. 0680	.1180	
997.00					.9820	.0520	.1360	. 0650		
995.00					.9320	.0540	.1390			
997.00					.9970	.0550	.1710			
1005,00				.05/0	1.0070	.0550	.1920			
1007,00				. 0360	.9980	.0540				
1015.00			.5660	.0350	.9940	.0520				
1017.00			.5940	.0370	1.0190	.0550	.2360			
1025.00		2.930	.5990	.0380	1.0170	.0570	.2460			
1037.00	1025.00	2.880	.5900	.0360	1.0360					
1035.00	1027.00	2.860	.5900	. 0360	1.6380					
1037.00		2.800	.5950	. 0350	1.0390					
1042.00	1037.00	2.790								
1045.00	1042.00	2.740	.5910							
1053.00	1045.00	2.710	.58 < 0							
1056.00	1053.00	2.650	.5450							
1064.00	1056.00	2.610	.5200							
1067.00	1064.00	2.530	.4860							
1073.00	1067.00		.4500							
1075.00	1073.00	2.510	.4150							
1084.00	1075.00	2.520								
1086.00	1084.00									
103.00	1086.00		.3430							
1103.00 2.730 .2960 .0460 1.0170 .0680 .1550 .0850 .1010 .1140 .105.00 2.840 .3100 .0440 1.0190 .0650 .1500 .0810 .1010 .1090 .115.00 2.860 .3120 .0440 1.0310 .0600 .1770 .0740 .1140 .1000 .121.00 2.980 .3250 .0410 1.0310 .0600 .1770 .0740 .1140 .1020 .121.00 2.980 .3250 .0410 1.0320 .0610 .1640 .0760 .1500 .1020 .124.00 3.020 .3410 .0390 1.0510 .0580 .1600 .0720 .1340 .0970 .133.00 3.060 .3470 .0400 1.0410 .0590 .1800 .0730 .1320 .0980 .135.00 3.120 .3650 .0410 1.0560 .0610 .1860 .0760 .1390 .1010 .144.00 3.150 .3940 .0390 1.0510 .0570 .2400 .0710 .1620 .0960 .144.00 3.150 .3940 .0390 1.0510 .0550 .0600 .2570 .0750 .1720 .1000 .0990	1095.00		.3090							
1113.00	1103.00									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1105.00	2.720	.2980							
1115.00	1113.00	2.840	.31110							
1121.00		2.860	.3120							
1124.00		2.980	.3200							
1133.00 3.060 .34/0 .0400 1.0410 .0590 .1800 .0/30 .1320 .1990 .135.00 3.120 .3650 .0410 1.0560 .0610 .1860 .0760 .1390 .1010 .144.00 3.150 .3940 .0390 1.0510 .0570 .2400 .0710 .1620 .0960 .147.00 3.170 .4220 .0400 1.0550 .0600 .2570 .0750 .1720 .1000 .0990	1124.00	3.020	.3410							
1135.00 3.120 .3650 .0410 1.0560 .0610 .1860 .0760 .1390 .1010 .1144.00 3.150 .3940 .0390 1.0510 .0570 .2400 .0710 .1620 .0960 .147.00 3.170 .4220 .0400 1.0550 .0600 .2570 .0750 .1720 .1000 .0560 .0560 .0560 .0560 .0560 .0560 .0600 .2570 .0750 .1720 .1000 .0600 .0600 .2570 .0750 .1720 .1000 .0600 .0600 .2570 .0750 .0750 .1000 .0600 .0		3.060	.34/0	.0400	1.0410					
1144.00 3.150 .3940 10390 1.0510 .0570 .2400 .0710 .1620 .0960 1147.00 3.170 .4220 .0400 1.0550 .0600 .2570 .0750 .1720 .1000			.3630	.0410						
1147.00 3.170 .4220 .0400 1.0550 .0600 .2570 .0750 .1720 .1000			.3940							
		3.170	.4220							
			.4360	.0370	1.0400	.0550	.2960	.0680	.2120	• 0450

TABLE VI (Contd.)

E _n , keV	σ _{el} , b	ω_1	$d\omega_1$	ω ₂	dω ₂	ω3	dw ₃	ω4	dω₄
1159.00	3.160	.4620	.0380	1.0340	.0560	.3140	.0690	.2110	.0930
1165.00	3.170	.4540	.0390	1.0220	.0590	.3350	.0720	.1990	.0980
1176.00	3.180	.4550	.0420	1.0520	.0630	.3240	.07/0	.2110	.1040
1179.00	3.160	.4650	. 0410	1.0450	.0610	.3310	.0760	.2010	.1010
1187.00	3.200	.4310	.0380	1.0580	.0570	.3490	.0700	.2000	.0940
1190.00	3.190	.4440	.0410	1.0700	.0620	.3550	. 0760	.2030	.1020
1197.00	3.170	.3730	.0430	1.0710	.0640	.3270	. 0790	.1790	.1070
1207.00	3.210	.38/0	.0400	1.0890	.0610	.3180	. 0740	.1900	.1000
1209.00	3.220	.38/0	.0410	1.0960	.0620	.3080	. 0760	.1830	.1020
1214.00	3.200	.3930	.0490	1.1030	.0730	.3040	.0900	.1670	.1210
1216.00	3.180	.3890	. 0490	1.1180	.0730	.2880	.0900	.1680	.1210
1224.00	3.180	.3860	.0460	1.1140	.0690	.2780	.0850	.1860	.1140
1226.00	3.180	.3990	.0480	1.1140	.0720	.2930	.0890	.1860	.1200
1234.00	3.150	.3//0	.0440	1.1090	.0650	.2610	.0800	.1910	.1090
1236.00	3.120	.3940	.0440	1.1080	.0650	.2570	.0810	.1910	.1090
1244.00	3.130	.3750	.0430	1.1170	.0640	.2430	.0790	.2010	.1060
1246.00	3.140	.3900	.0450	1.1290	.0670	.2340	.0820	.1980	.1110
1254.00	3.210	.3650	.0430	1.1310	.0640	.2310	. 0780	.2010	.1060
1256.00	3.180	.3760	.0440	1.1430	.0660	.2280	.0810	.2080	.1100
1259.00	3.180	.3860	.0450	1.1480	.0670	.2240	.0820	.2120	.1110
1267.00	3.190	.3590	.0440	1.1540	.0660	.2190	.0810	.2010	.1100
1272.00	3.190	.3320	.0350	1.1610	.0530	.2280	.0640	.2000	.0880
1275.00	3.200	.30/0	.0350	1.1560	.0520	.2260	.0640	.1980	.0870
1283.00	3.150	.3460	.0340	1.1530	.0520	.2640	.0630	.1980	.0870
1286.00	3.120	.3500	.0350	1.1810	.0530	.2580	.0640	.1/60	.0880
1292.00	3.160	.34/0	.0380	1.1870	.0560	.2670	.0690	.1760	.0940
1294.00	3.140	.3610	.0380	1.1950	.0570	.2600	.0700	.1660	.0970
1301.00	3.160	.3650	.0390	1.1900	.0590	.2540	.0720	.1620	.0990
1303.00	3.080	.3890	.0380	1.1940	.0570	.2650	.0700	.1570	.0970
1307.00	3.050	.41/0	.0390	1.1870	.0580	.2760	.0710	.1760	.0980
1310.00	3.000	.4220	.0400	1.1530	.0600	.2540	.0740	.1490	.1010
1320.00	3.060	.4450	.0410	1.1750	.0610	.2850	.0750	.1920	.1030
1330.00	3.080	.4600	.0430	1.1850	.0650	.3000	.0790	.2200	.1090
1334.00	3.110	.4260	. 0480	1.1960	.0710	.2520	. 08/0	.2010	.1190
1350.00	3.150	.4400	.0420	1.1780	.0630	.2480	.0770	.1920	.1060
1360.00	3.190	.4810	.0420	1.1270	.0630	.3160	.07/0	.1880	.1060
1376.00	3.200	.4880	.04/0	1.1130	.0710	.3120	. U860	.1640	.1180
1386.00	3.150	.4900	.0550	1.1080	.0820	.3500	.1000	.1790	.1380
1393.00	3.230	.4900	. 0570	1.1040	.0850	.3570	.1040	.1580	.1420
1396.00	3.270	.4890	.0620	1.1160	.0920	.3520	.1120	.1660	.1540
1406.00	3.240	.4940	.0560	1.1020	.0860	.3700	.1050	.1580	.1450
1413.00	3.270	.5240	. 0560	1.1130	.0840	.3530	.1020	.1610	.1400
1416.00	3.280	.5390	.0570	1.1270	.0860	.3840	.1050	.2030	.1440

E _n , keV	σ _{el} , b	ω_1	$d\omega_1$	w ₂	dωz	ω_3	$d\omega_3$	ω4	d ω ₄
1426.00	3.260 3.270	.5040 .5290	.0510 .0520	1.1310	.0770	.3650 .4110	.0940	.1920 .2130	.1290 .1300
1436.00	3.270	.5450 .5030	.0500 .0420	1.1460	.0760	.4310 .3750	.0920	.2290	.1260 .1050
1447.00	3.220	.5040	.0380 .0390	1.1230	.0570	.3620	.0690	.1940	0950
1460.00	3.360	.4920	.0410 .0430	1.1460	.0610	.3590 .3660	.0740	.2600	.1020 .1080
1467.00	3.340	.3980	0370	1.1890	.0550	.3460	.0680	.3080	.0930

TABLE VII. Cross Sections for the Inelastic Excitations of the 320-keV State in Vanadium by Neutron Scattering

En, MeV	o _{in} , b	doin, b	E _n , MeV	o _{in} , b	doin, b
.650	.330	.054	.6500	.2031	.0391
.674	.389	.056	.6775	.3865	.0661
.686	.406	.051	. 6953	.3932	.0372
.695	.475	.049	./050	.4207	.0539
.716	.383	.039	.7259	.3735	.0274
.727	.388	.032	.1339	.3/18	.0275
.734	.356	.027	./366	. 3746	.0332
.740	.371	.040	. 1400	.4750	.0/10
.753	.333	.023	. /550	. 3345	.0251
.756	.343	.029	.7659	.3526	.0248
.767	.351	.028	. 1759	.4281	.0302
.774	.463	.035	.7766	.4649	.0412
.785	.480	.037	.7866	.4504	.0403
.794	.494	.038	.7966	,5551	.0481
.804	.512	.039	.8066	.4657	.0434
.813	.509	.045	,8149	.6041	.0640
.827	.513	.039	, 8339	.4900	.0332
.834	.513	.038	.8366	.5242	.0455
.844	.487	.035	.3466	.4904	.0403
.854	.495	.036	.8566	.5162	.0452
.865	.474	.031	.8674	.4399	.0324
.873	.440	.029	.8749	.4443	.0333
.876	.432	.037	. 6849	.3943	.0302
.886	.385	.034	.8949	.3918	.0300
.896	.408	.035	.9049	.3987	.0300
.906	.402	.035	.9149	.3496	.0262
.916	.337	.029	,9249	.3660	.0276
.926	.384	.033	.9349	.4362	.0328
.936	.452	.039	.9453	.4687	.0406
.944	.469	.049	.9566	.4317	.0375
,963	.405	.035	. 9649	.4185	.0444
.976	.372	.032	.9849	.3827	.0287
.986	.392	.034	, 9899	.4016	.0426
.989	.415	.062	1.0050	,3933	.0296
1.006	.400	.034	1.0100	.3951	.0423
1.010	.336	.050	1.0200	.4433	.0385
1.035	.419	.031	1.0360	.4097	.0356
1.043	.405	.035	1.0450	,3820	.0474
1.055	.432	.046	1.0650	.4468	.0317
1.076	.428	.037	1.0850	.4226	.001/

		1 h	E _n , MeV	o _{in} , b	dσ _{in} , b
E _n , MeV	o _{in} , b	dσ _{in} , b	Dn, 1110		
		.036	1.0950	.4223	.0286
1.086	.416	.032	1,1000	.4458	.0301
1.097	. 433		1.1060	.4617	.0400
1.104	.445	.033	1.1160	.5064	.0438
1.115	.485	.036	1.1200	.4850	. 0420
1.124	.492	.036	1.1550	,5220	. 0556
1.133	.510	.044	1.1500	.4822	.0421
1.145	.558	.059	1.1650	.4567	.0469
1.163	.420	.036	1.1830	.3933	.0340
1.176	.389	.033	1.1950	.4294	.0290
1.185	.397	.042	1.2040	.4300	.0265
1.197	.443	.033	1.2070	.4380	.0331
1.205	.438	.029		.4081	.0274
1.214	.401	.024	1.2150	.4275	.0263
1.217	.407	.030	1.2240	.4461	.0336
1.225	.427	.028	1.2270	.4428	.0334
1.233	. 438	.029	1.2350	.4015	.0425
1.236	.412	.035	1.2400	.4133	.0279
1.240	.413	.061	1.2540	.4173	.0363
1.255	.400	.030	1.2560	.3924	.0341
1.265	.409	.030	1.2660		.0423
1.274	.470	.035	1.2760	.4789	.0547
1.283	.547	.047	1.2850	.5108	.0323
1.296	.520	.045	1.3050	.4811	
1.307	.490	.0.56	1.3120	.4640	.0349
1.313	.451	.039	1.3150	.4656	.0495
1.325	.408	.043	1.3300	.3912	.0586
1.353	.436	.029	1.3540	.4259	.0319
1.356	.424	.036	1,3650	.4256	.0322
1.366	.429	.037	1.3730	.4178	.0367
1.374	.367	.038	1.3860	.4403	.0385
1.395	.448	.034	1.4010	.4465	.0306
1.395	.429	.046	1.4060	.3864	.0336
1.413	.400	.034	1.4150	.3860	.0410
1.426	.399	.034	1.4330	.4016	.0348
1.435	.382	.040	1.44/0	.36/3	.0291
1.453	.387	.026	1,4550	.3827	.0289
1.456	.369	.032	1.4640	.3931	.0297
1.466	.419	.036	1.4750	.4069	.0353
1.475	.384	.040	1,4860	.4052	.0351
1.490	.406	.043	1,4900	.3950	.0593

TABLE VIII. Cross Sections for the Inelastic Neutron Excitations of the 930-keV State in Vanadium

E _n , MeV	σ _{in} , b	dσ _{in} , b
1.250	.094	.057
1.300	.0850	.0186
1.350	.175	.040
1.360	.1603	.0693
1.400	.145	.021
1.4100	.1025	.0258
1.450	.125	.019
1.4650	.1438	.0673
1.500	.998	.027

ACKNOWLEDGMENTS

We acknowledge the assistance of a number of members of Argonne National Laboratory staff. We are particularly indebted to Dr. P. A. Moldauer for theoretical assistance and guidance.

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